International TOR Rectifier

IRF7807PbF IRF7807APbF

HEXFET® Chip-Set for DC-DC Converters

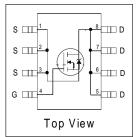
- N Channel Application Specific MOSFETs
- · Ideal for Mobile DC-DC Converters
- Low Conduction Losses
- · Low Switching Losses
- Lead-Free

Description

These new devices employ advanced HEXFET Power MOSFET technology to achieve an unprecedented balance of on-resistance and gate charge. The reduced conduction and switching losses make them ideal for high efficiency DC-DC Converters that power the latest generation of mobile microprocessors.

A pair of IRF7807 devices provides the best cost/performance solution for system voltages, such as 3.3V and 5V.





Device Features

| | IRF7807 | IRF7807A |
|---------|---------------------|--------------|
| Vds | 30V | 30V |
| Rds(on) | $25 \text{m}\Omega$ | $25 m\Omega$ |
| Qg | 17nC | 17nC |
| Qsw | 5.2nC | |
| Qoss | 16.8nC | 16.8nC |

Absolute Maximum Ratings

| Parameter | Symbol | IRF7807 | IRF7807A | Units | |
|---------------------------------------|-----------------|-----------------|------------|-------|----|
| Drain-Source Voltage | V _{DS} | 3 | V | | |
| Gate-Source Voltage | V_{gs} | ±′ | | | |
| Continuous Drain or Source | 25°C | I _D | 8.3 | 8.3 | Α |
| Current (V _{GS} ≥ 4.5V) 70°C | | | 6.6 | 6.6 | |
| Pulsed Drain Current① | | I _{DM} | 66 | 66 | |
| Power Dissipation 25°C | | P _D | 2 | W | |
| | | 1. | .6 | | |
| Junction & Storage Temperature Range | | T_{J},T_{STG} | -55 to 150 | | °C |
| Continuous Source Current (F | I _s | 2.5 | 2.5 | Α | |
| Pulsed source Current | I _{SM} | 66 | 66 | | |

Thermal Resistance

| Parameter | | Max. | Units |
|------------------------------|--------------------|------|-------|
| Maximum Junction-to-Ambient® | $R_{_{\theta JA}}$ | 50 | °C/W |

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| Electrical Characteristics | | IRF7807 | | | IRF7807A | | |] | |
|---------------------------------------|----------------------|---------|------|------|-------------|------|-------|------------|---|
| Parameter | | Min | Тур | Max | Min Typ Max | | Units | Conditions | |
| Drain-to-Source Breakdown Voltage* | V _{(BR)DSS} | 30 | - | _ | 30 | _ | - | V | $V_{GS} = 0V$, $I_D = 250\mu A$ |
| Static Drain-Source on Resistance* | R _{DS} (on) | | 17 | 25 | | 17 | 25 | mΩ | $V_{GS} = 4.5V, I_{D} = 7A@$ |
| Gate Threshold Voltage* | V _{GS} (th) | 1.0 | | | 1.0 | | | V | $V_{DS} = V_{GS}, I_{D} = 250 \mu A$ |
| Drain-Source Leakage | I _{DSS} | | | 30 | | | 30 | μА | $V_{DS} = 24V, V_{GS} = 0$ |
| Current* | | | | 150 | | | 150 | | $V_{DS} = 24V, V_{GS} = 0,$ Tj = 100°C |
| Gate-Source Leakage Current* | I _{GSS} | | | ±100 | | | ±100 | nA | V _{GS} = ±12V |
| Total Gate Charge* | Q _g | | 12 | 17 | | 12 | 17 | | $V_{GS} = 5V, I_D = 7A$ |
| Pre-Vth Gate-Source Charge | Q _{gs1} | | 2.1 | | | 2.1 | | | $V_{DS} = 16V, I_{D} = 7A$ |
| Post-Vth Gate-Source Charge | Q _{gs2} | | 0.76 | | | 0.76 | | nC | |
| Gate to Drain Charge | Q_{gd} | | 2.9 | | | 2.9 | | | |
| Switch Charge* $(Q_{gs2} + Q_{gd})$ | Q _{sw} | | 3.66 | 5.2 | | 3.66 | | | |
| Output Charge* | Q _{oss} | | 14 | 16.8 | | 14 | 16.8 | | $V_{DS} = 16V, V_{GS} = 0$ |
| Gate Resistance | R _g | | 1.2 | | | 1.2 | | Ω | |
| Turn-on Delay Time | t _d (on) | | 12 | | | 12 | | | $V_{DD} = 16V$ |
| Rise Time | t _r | | 17 | | | 17 | | ns | $I_D = 7A$ |
| Turn-off Delay Time | t _d (off) | | 25 | | | 25 | | | $R_g = 2\Omega$ |
| Fall Time | t _f | | 6 | | | 6 | | | V _{GS} = 4.5V Resistive Load |

Source-Drain Rating & Characteristics

| Parameter | | Min | Тур | Max | Min | Тур | Max | Units | Conditions |
|--|--------------------|-----|-----|-----|-----|-----|-----|-------|--|
| Diode Forward Voltage* | V _{SD} | | | 1.2 | | | 1.2 | V | $I_S = 7A \odot$, $V_{GS} = 0V$ |
| Reverse Recovery Charge® | Q _{rr} | | 80 | | | 80 | | nC | di/dt = $700A/\mu s$ $V_{DS} = 16V, V_{GS} = 0V, I_{S} = 7A$ |
| Reverse Recovery Charge (with Parallel Schotkky) | Q _{rr(s)} | | 50 | | | 50 | | | di/dt = $700A/\mu s$ (with $10BQ040$) $V_{DS} = 16V$, $V_{GS} = 0V$, $I_{S} = 7A$ |

- Repetitive rating; pulse width limited by max. junction temperature.
 Pulse width ≤ 300 µs; duty cycle ≤ 2%.
 When mounted on 1 inch square copper board, t < 10 sec.
 Typ = measured Q_{oss}
 Devices are 100% tested to these parameters.

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Power MOSFET Selection for DC/DC Converters

Control FET

Special attention has been given to the power losses in the switching elements of the circuit - Q1 and Q2. Power losses in the high side switch Q1, also called the Control FET, are impacted by the $R_{\mbox{\tiny ds(on)}}$ of the MOSFET, but these conduction losses are only about one half of the total losses.

Power losses in the control switch Q1 are given by;

$$P_{loss} = P_{conduction} + P_{switching} + P_{drive} + P_{output}$$

This can be expanded and approximated by;

$$\begin{split} P_{loss} &= \left(I_{rms}^{2} \times R_{ds(on)}\right) \\ &+ \left(I \times \frac{Q_{gd}}{i_{g}} \times V_{in} \times f\right) + \left(I \times \frac{Q_{gs2}}{i_{g}} \times V_{in} \times f\right) \\ &+ \left(Q_{g} \times V_{g} \times f\right) \\ &+ \left(\frac{Q_{oss}}{2} \times V_{in} \times f\right) \end{split}$$

This simplified loss equation includes the terms $Q_{\rm gs2}$ and $Q_{\rm oss}$ which are new to Power MOSFET data sheets.

 Q_{gs2} is a sub element of traditional gate-source charge that is included in all MOSFET data sheets. The importance of splitting this gate-source charge into two sub elements, Q_{gs1} and Q_{gs2} , can be seen from Fig 1.

 Q_{gs2} indicates the charge that must be supplied by the gate driver between the time that the threshold voltage has been reached (t1) and the time the drain current rises to I_{dmax} (t2) at which time the drain voltage begins to change. Minimizing Q_{gs2} is a critical factor in reducing switching losses in Q1.

 $Q_{\scriptscriptstyle oss}$ is the charge that must be supplied to the output capacitance of the MOSFET during every switching cycle. Figure 2 shows how $Q_{\scriptscriptstyle oss}$ is formed by the parallel combination of the voltage dependant (non-linear) capacitance's $C_{\scriptscriptstyle ds}$ and $C_{\scriptscriptstyle dg}$ when multiplied by the power supply input buss voltage.

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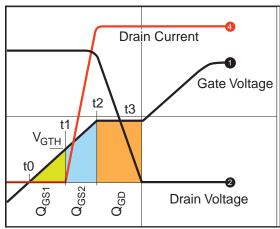


Figure 1: Typical MOSFET switching waveform

Synchronous FET

The power loss equation for Q2 is approximated by;

$$\begin{split} P_{loss} &= P_{conduction} + P_{drive} + P_{output}^* \\ P_{loss} &= \left(I_{rms}^2 \times R_{ds(on)}\right) \\ &+ \left(Q_g \times V_g \times f\right) \\ &+ \left(\frac{Q_{oss}}{2} \times V_{in} \times f\right) + \left(Q_{rr} \times V_{in} \times f\right) \end{split}$$

*dissipated primarily in Q1.

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For the synchronous MOSFET Q2, R $_{\rm ds(on)}$ is an important characteristic; however, once again the importance of gate charge must not be overlooked since it impacts three critical areas. Under light load the MOSFET must still be turned on and off by the control IC so the gate drive losses become much more significant. Secondly, the output charge $Q_{\rm oss}$ and reverse recovery charge $Q_{\rm r}$ both generate losses that are transfered to Q1 and increase the dissipation in that device. Thirdly, gate charge will impact the MOSFETs' susceptibility to Cdv/dt turn on.

The drain of Q2 is connected to the switching node of the converter and therefore sees transitions between ground and V_{in}. As Q1 turns on and off there is a rate of change of drain voltage dV/dt which is capacitively coupled to the gate of Q2 and can induce a voltage spike on the gate that is sufficient to turn

the MOSFET on, resulting in shoot-through current . The ratio of $Q_{\rm gd}/Q_{\rm gs1}$ must be minimized to reduce the potential for Cdv/dt turn on.

Spice model for IRF7807 can be downloaded in machine readable format at www.irf.com.

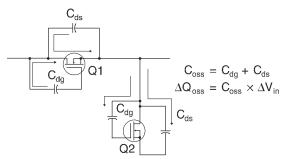
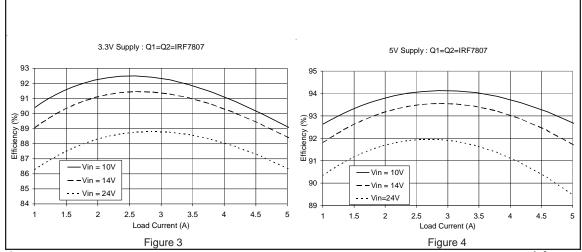
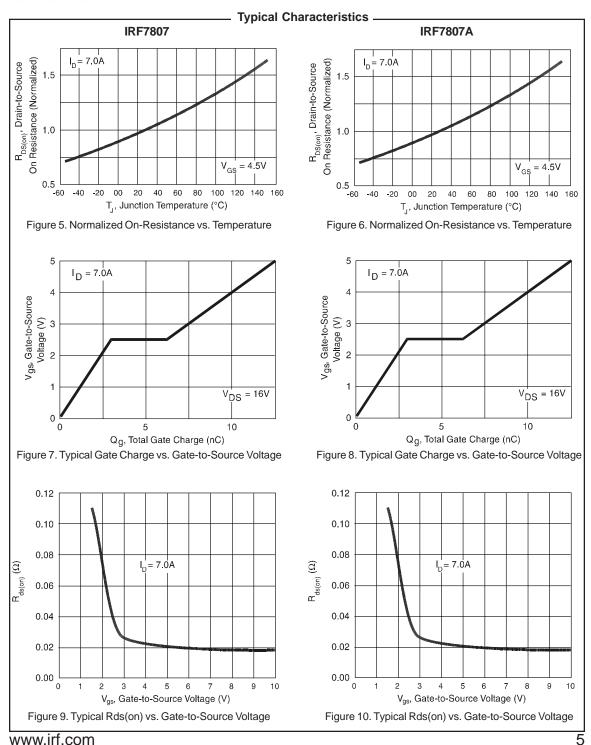


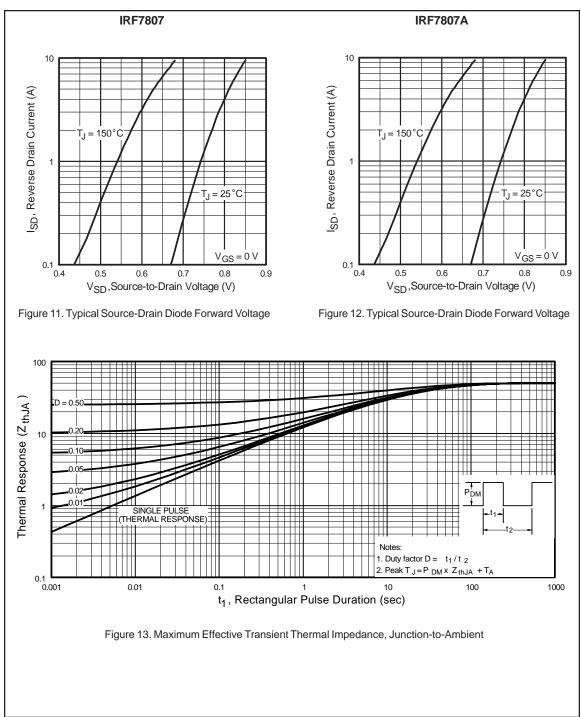
Figure 2: Qoss Characteristic

Typical Mobile PC Application

The performance of these new devices has been tested in circuit and correlates well with performance predictions generated by the system models. An advantage of this new technology platform is that the MOSFETs it produces are suitable for both control FET and synchronous FET applications. This has been demonstrated with the 3.3V and 5V converters. (Fig 3 and Fig 4). In these applications the same MOSFET IRF7807 was used for both the control FET (Q1) and the synchronous FET (Q2). This provides a highly effective cost/performance solution.





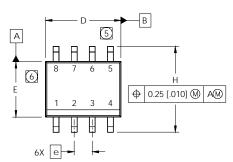


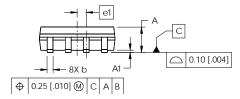
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SO-8 Package Outline

Dimensions are shown in millimeters (inches)

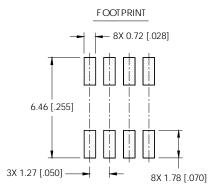




y 7 8X L 8X C

NOTES:

- 1. DIMENSIONING & TOLERANCING PER ASME Y14.5M-1994.
- 2. CONTROLLING DIMENSION: MILLIMETER
- 3. DIMENSIONS ARE SHOWN IN MILLIMETERS [INCHES].
- 4. OUTLINE CONFORMS TO JEDEC OUTLINE MS-012AA.
- (5) DIMENSION DOES NOT INCLUDE MOLD PROTRUSIONS. MOLD PROTRUSIONS NOT TO EXCEED 0.15 [.006].
- (6) DIMENSION DOES NOT INCLUDE MOLD PROTRUSIONS. MOLD PROTRUSIONS NOT TO EXCEED 0.25 [.010].
- [7] DIMENSION IS THE LENGTH OF LEAD FOR SOLDERING TO A SUBSTRATE.



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MILLIMETERS

MIN MAX

1.75 0.25

0.51

0.25

5.00

4.00

6.20

0.50

1.27

1 35

0.10

0.19

4.80

3.80

5.80

0.40

1.27 BASIC

0.635 BASIC

INCHES

MAX

0688

.0098

.020

0098

.1574

2440

.0196

.050

MIN

.0075

2284

.0099

.016

0°

.050 BASIC

.025 BASIC

DIM

A .0532

A1 .0040

b .013

С

D .189

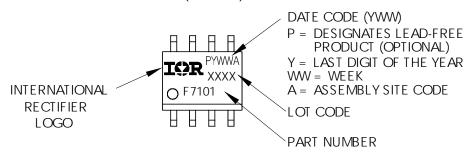
E .1497

е

Н

SO-8 Part Marking

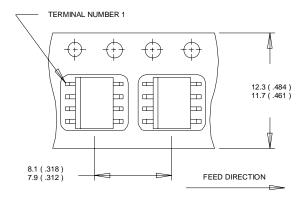
EXAMPLE: THIS IS AN IRF7101 (MOSFET)



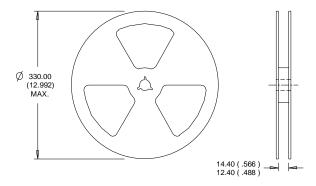
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SO-8 Tape and Reel

Dimensions are shown in millimeters (inches)



- 1. CONTROLLING DIMENSION: MILLIMETER.
 2. ALL DIMENSIONS ARE SHOWN IN MILLIMETERS(INCHES).
- OUTLINE CONFORMS TO EIA-481 & EIA-541.



- CONTROLLING DIMENSION : MILLIMETER.
 OUTLINE CONFORMS TO EIA-481 & EIA-541.

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