

7.0V to 26V Input, 1.0A, Integrated MOSFET Single Synchronous Buck DC/DC Converter





0 μA (Typ.)

BD9E102FJ

General Description

The BD9E102FJ is a synchronous buck switching regulator with low on-resistance built-in power MOSFETs. High efficiency at light load with a SLLMTM. It is most suitable for use in the equipment to reduce the standby power is required. It is a current mode control DC/DC converter and features high-speed transient response. Phase compensation can also be set easily.

Features

- Synchronous single DC/DC converter
- SLLMTM control (Simple Light Load Mode)
- Efficiency = 80% (@lout=10mA)
- Over current protection
- Short circuit protection
- Thermal shutdown protection
- Undervoltage lockout protection
- Soft start
- Reduce external diode
- SOP-J8 package

Applications

- Consumer applications such as home appliance
- Secondary power supply and Adapter equipments
- Telecommunication devices

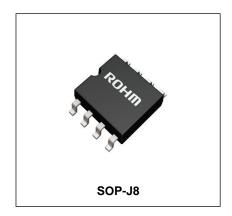
Key Specifications

Input voltage range: 7.0V to 26V
 Adjustable output voltage range: 1.0V to VIN x 0.7V
 Maximum output current: 1.0 A (Max.)
 Switching frequency: 570 kHz (Typ.)
 High-Side MOSFET on-resistance: 250 mΩ (Typ.)
 Low-Side MOSFET on-resistance: 200 mΩ (Typ.)

Package W (T SOP-J8 4.90

Shutdown current:

W (Typ.) x D (Typ.) x H (Max.) 4.90 mm x 6.00 mm x 1.65 mm



Typical Application Circuit

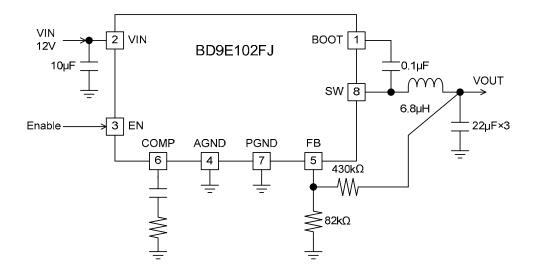


Figure 1. Application circuit

Pin Configuration

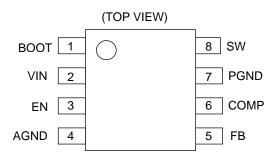


Figure 2. Pin assignment

Pin Descriptions

| Pin No. | Pin Name | Description | | | |
|---|----------|---|--|--|--|
| 1 | BOOT | Connect a bootstrap capacitor of 0.1 μ F between this terminal and SW terminals. The voltage of this capacitor is the gate drive voltage of the high-side MOSFET. | | | |
| 2 | VIN | Power supply terminal for the switching regulator and control circuit. Connecting a 10 µF ceramic capacitor is recommended. | | | |
| 3 | EN | Turning this terminal signal low-level (0.8 V or lower) forces the device to enter the shut down mode. Turning this terminal signal high-level (2.0 V or higher) enables the device. This terminal must be terminated. | | | |
| 4 | AGND | Ground terminal for the control circuit. | | | |
| 5 | FB | Inverting input node for the gm error amplifier. See page 22 for how to calculate the resistance of the output voltage setting. | | | |
| 6 | COMP | Input terminal for the gm error amplifier output and the output switch current comparator. Connect a frequency phase compensation component to this terminal. See page 22 for how to calculate the resistance and capacitance for phase compensation. | | | |
| 7 | PGND | Ground terminals for the output stage of the switching regulator. | | | |
| drain of the low-side MOSFET. Connect a bootstrap capacitor of 0.1 µF between | | Switch node. This terminal is connected to the source of the high-side MOSFET and drain of the low-side MOSFET. Connect a bootstrap capacitor of 0.1 μ F between these terminals and BOOT terminals. In addition, connect an inductor of 6.8 μ H with attention paid to theconsidering the direct current superimposition characteristic. | | | |

Block Diagram

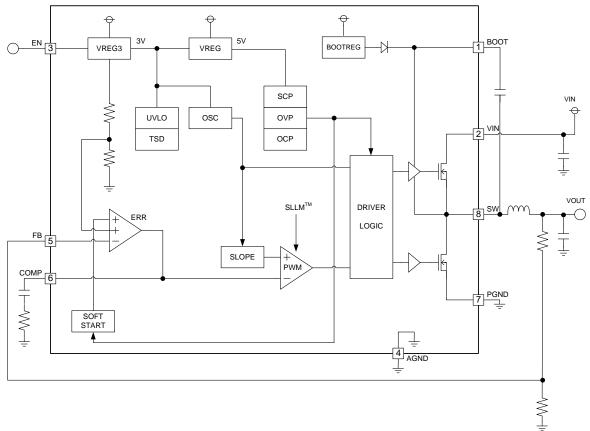


Figure 3. Block diagram

Description of Blocks

VREG3

Block creating internal reference voltage 3V (typ.).

VRFG

Block creating internal reference voltage 5V (typ.).

BOOTREG

Block creating gate drive voltage.

TSD

This is thermal shutdown block. Thermal shutdown circuit shuts down when inner part of IC becomes more than 175°C (typ.). Also when the temperature degrease it returns with hysteresis of 25°C(typ.).

UVLO

This is under voltage lockout block. IC shuts down with VIN under 6.4V (typ.). Still the threshold voltage has hysteresis of 200mV (typ.).

ERR

Circuit to compares the feedback voltage of standard and output voltage. Switching duty is settled by this compared result and COMP terminal voltage. Also, because soft start occurs at activation, COMP terminal voltage is controlled by internal slope voltage.

OSC

Block generating oscillation frequency.

SLOPE

Creates delta wave from clock, generated by OSC, and sends voltage composed by current sense signal of high side MOSFET and delta wave to PWM comparator.

PWM

Settles switching duty by comparing output COMP terminal voltage of error amplifier and signal of SLOPE part.

DRIVER LOGIC

This is DC/DC driver block. Input signal from PWM and drives MOSFET.

SOFT START

By controlling current output voltage starts calmly preventing over shoot of output voltage and inrush current.

OCP

Current flowing in high side MOSFET is controlled one circle each of switching frequency when over current occurs.

SCF

The short circuit protection block compares the FB terminal voltage with the internal standard voltage VREF. When the FB terminal voltage has fallen below 0.56 V (typ.) and remained there for 0.9 msec (typ.), SCP stops the operation for 14.4 msec (typ.) and subsequently initiates a restart.

OVP

Over voltage protection function (OVP) compares FB terminal voltage with the internal standard voltage VREF. When the FB terminal voltage exceeds 1.04V (typ.) it turns MOSFET of output part MOSFET OFF. After output voltage drop it returns with hysteresis.

◆ Absolute Maximum Ratings (Ta = 25°C)

| Parameter | Symbol | Rating | Unit |
|-------------------------------------|--------|-------------|------|
| Supply Voltage | VIN | -0.3 to +30 | V |
| EN Input Voltage | VEN | -0.3 to +30 | V |
| Voltage from GND to BOOT | Vвоот | -0.3 to +35 | V |
| Voltage from SW to BOOT | ⊿Vвоот | -0.3 to +7 | V |
| FB Input Voltage | VFB | -0.3 to +7 | V |
| COMP Input Voltage | VCOMP | -0.3 to +7 | V |
| SW Input Voltage | Vsw | -0.5 to +30 | V |
| Output Current | Іоит | 1.0 | Α |
| Allowable Power Dissipation | Pd | 0.675*1 | W |
| Operating Ambient Temperature Range | Topr | -40 to +85 | °C |
| Storage Temperature Range | Tstg | -55 to +150 | °C |

^{*1} When mounted on a 70 mm x 70 mm x 1.6 mm 1-layer glass epoxy board Derated by 5.4 mW/ $^{\circ}$ C for Ta \geq 25 $^{\circ}$ C.

Recommended Operating Ratings

| Parameter | Symbol | | - Unit | | |
|----------------------|--------|-------|--------|-----------|-------|
| Farameter | | Min | Тур | Max | UIIII |
| Supply Voltage | VIN | 7.0 | - | 26 | V |
| Output Current | lout | - | - | 1.0 | Α |
| Output Voltage Range | VRANGE | 1.0*2 | - | VIN × 0.7 | V |

^{*2} Please use it in I/O voltage setting of which output pulse width does not become 250nsec (typ.) or less. See the page 22 for how to calculate the resistance of the output voltage setting.

Electrical Characteristics

(Ta = 25°C, V_{IN} = 12 V, V_{EN} = 3 V unless otherwise specified)

| Doromotor | Cumbal | Limits | | | Lloit | Conditions |
|-----------------------------|----------|--------|-------|-----------------|-------|-------------|
| Parameter | Symbol | Min | Тур | Max | Unit | Conditions |
| Supply Current in Operating | lopr | - | 250 | 500 | μΑ | VFB = 0.9V |
| Supply Current in Standby | Istby | - | 0 | 10 | μA | VEN = 0V |
| Reference Voltage | VFB | 0.784 | 0.800 | 0.816 | V | |
| FB Input Current | lfв | -1 | 0 | 1 | μA | VFB = 0V |
| Switching frequency | Fosc | 484 | 570 | 656 | kHz | |
| Maximum Duty ratio | Maxduty | 88 | 93 | 98 | % | |
| High-side FET on-resistance | Ronh | - | 250 | - | mΩ | Isw = 100mA |
| Low-side FET on-resistance | Ronl | - | 200 | - | mΩ | Isw = 100mA |
| Over Current limit | ILIMIT | 1.9 | 2.2 | 2.5 | Α | |
| UVLO detection voltage | Vuvlo | 6.1 | 6.4 | 6.7 | V | Vin falling |
| UVLO hysteresis voltage | Vuvlohys | 100 | 200 | 300 | mV | |
| EN high-level input voltage | VENH | 2.0 | - | V _{IN} | V | |
| EN low-level input voltage | VENL | - | - | 0.8 | V | |
| EN Input current | len | 2 | 4 | 8 | μA | VEN = 3V |
| Soft Start time | Tss | 1.2 | 2.5 | 5.0 | msec | |
| | | | | | | |

- VFB: FB Input Voltage. VEN: EN Input Voltage.
- Pd should not be exceeded.

Typical Performance Curves

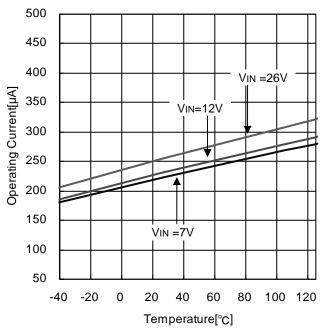


Figure 4. Operating Current - Temperature

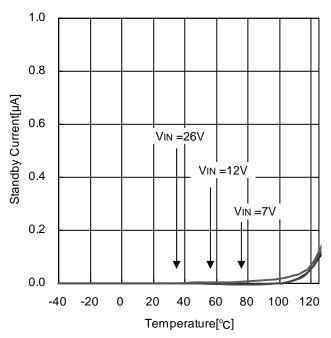


Figure 5. Stand-by Current - Temperature

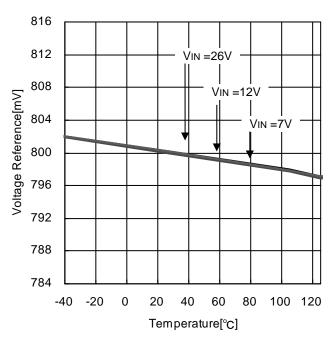


Figure 6. FB Voltage Reference - Temperature

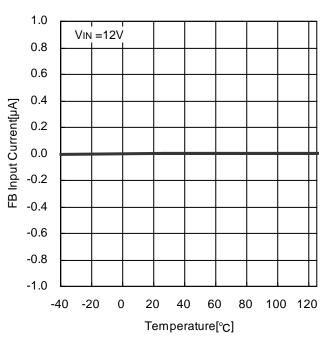


Figure 7. FB Input Current - Temperature

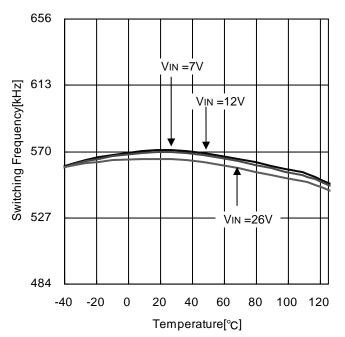


Figure 8. Switching Frequency - Temperature

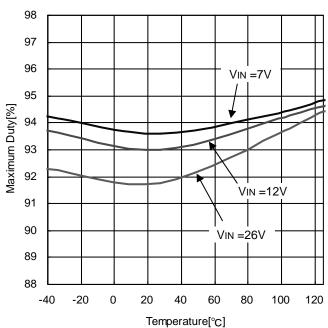


Figure 9. Maximum Duty - Temperature

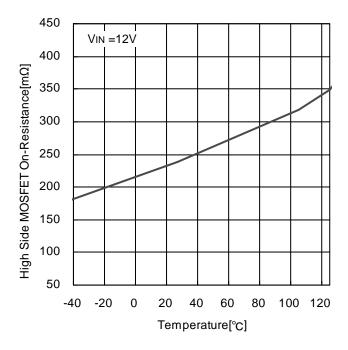


Figure 10. High Side MOSFET On-Resistance-Temperature

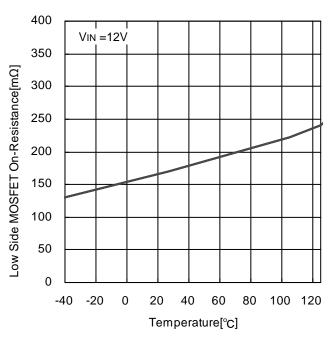


Figure 11. Low Side MOSFET On-Resistance-Temperature

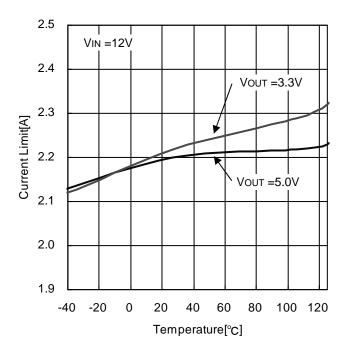


Figure 12. Current Limit - Temperature

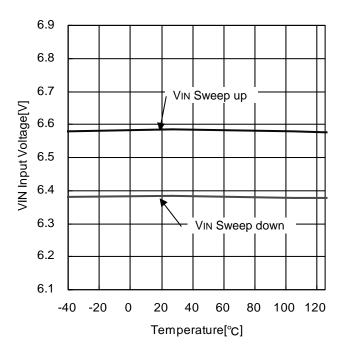


Figure 13. UVLO Threshold - Temperature

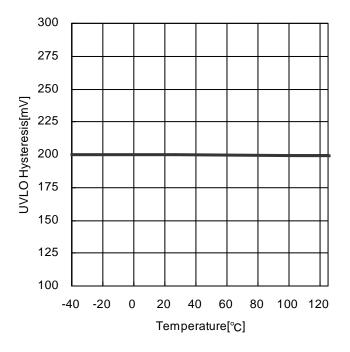


Figure 14. UVLO Hysteresis-Temperature

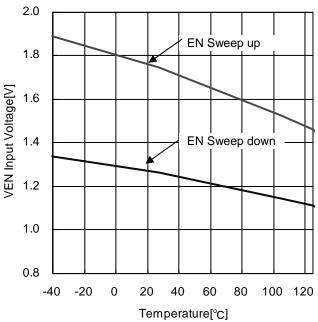
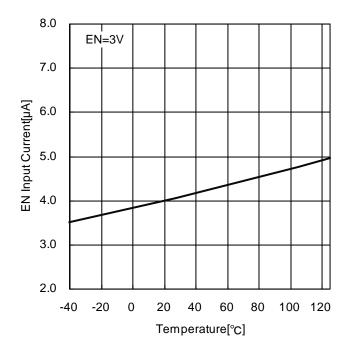
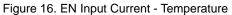


Figure 15. EN Threshold - Temperature





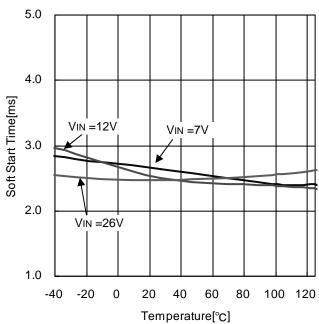


Figure 17. Soft Start Time - Temperature

● Typical Performance Curves (Application)

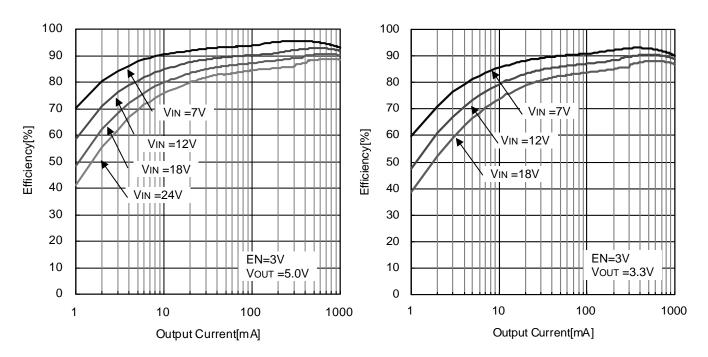


Figure 18. Efficiency - Output Current (VOUT = 5.0V)

Figure 19. Efficiency - Output Current (VOUT = 3.3V)

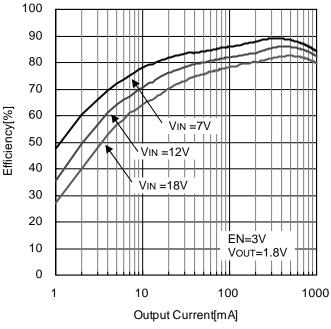


Figure 20. Efficiency - Output Current (Vout = 1.8V)

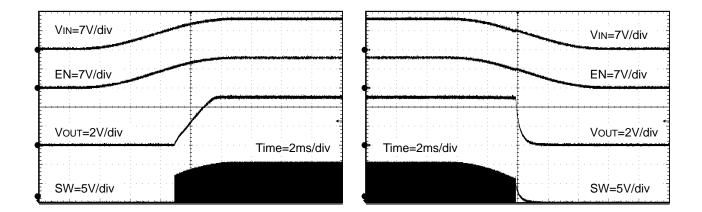


Figure 21. Power Up (VIN = EN)

Figure 22. Power Down (VIN = EN)

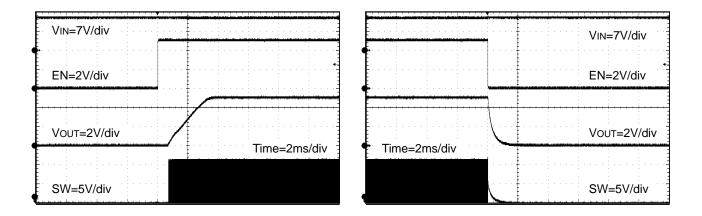
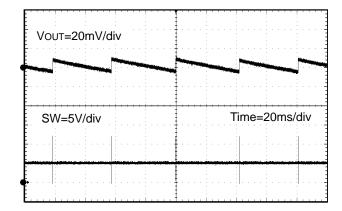


Figure 23. Power Up (EN = $0V \rightarrow 5V$)

Figure 24. Power Down (EN = 5V→0V)



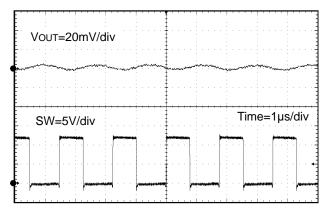
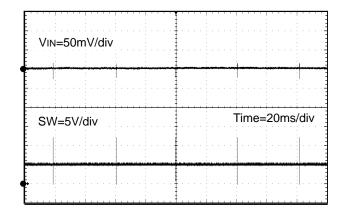


Figure 25. Vout Ripple (VIN = 12V, Vout = 5V, Iout = 0A)

Figure 26. VOUT Ripple (VIN = 12V, VOUT = 5V, IOUT = 1A)



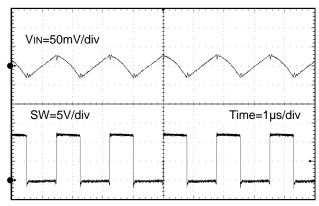
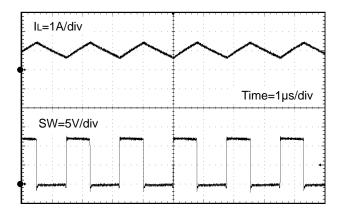


Figure 27. VIN Ripple (VIN = 12V, VOUT = 5V, IOUT = 0A)

Figure 28. VIN Ripple (VIN = 12V, VOUT = 5V, IOUT = 1A)



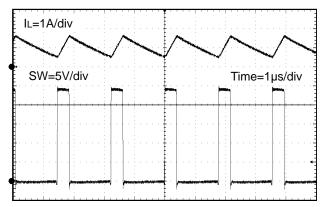


Figure 29. Switching Waveform (VIN = 12V, VOUT = 5V, IOUT = 1A)

Figure 30. Switching Waveform (VIN = 24V, VOUT = 5V, IOUT = 1A)

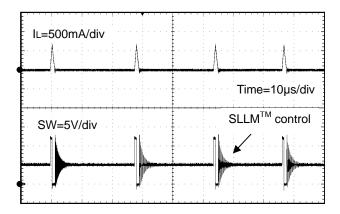
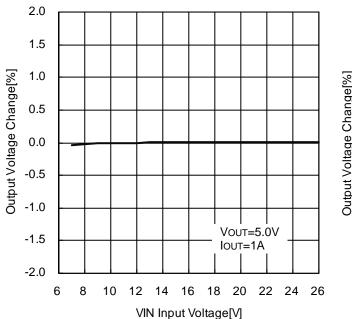


Figure 31. Switching Waveform (VIN = 12V, VOUT = 5V, IOUT = 20mA)



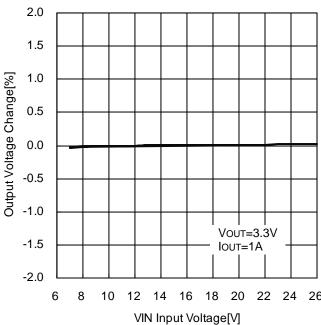


Figure 32. Vout Line Regulation (Vout = 5.0V)

Figure 33. VouT Line Regulation (VouT = 3.3V)

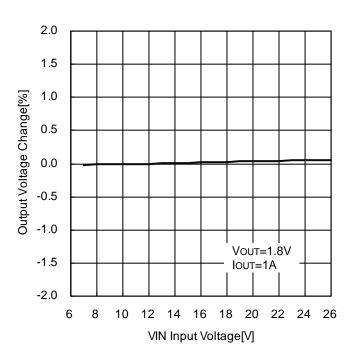
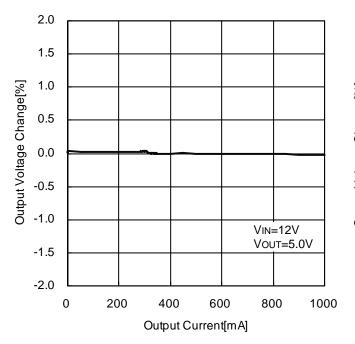


Figure 34. Vout Line Regulation (Vout = 1.8V)



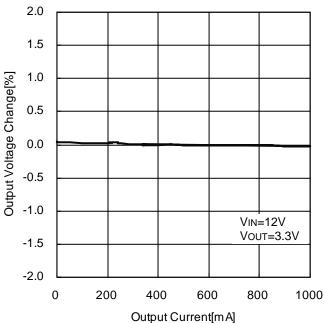


Figure 35. Vout Load Regulation (Vout = 5.0V)

Figure 36. Vout Load Regulation (Vout = 3.3V)

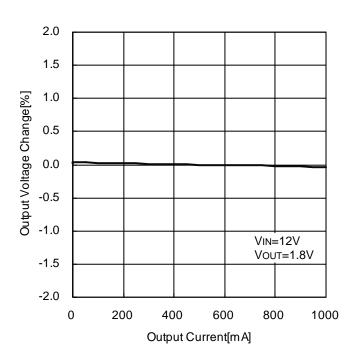


Figure 37. Vout Load Regulation (Vout = 1.8V)

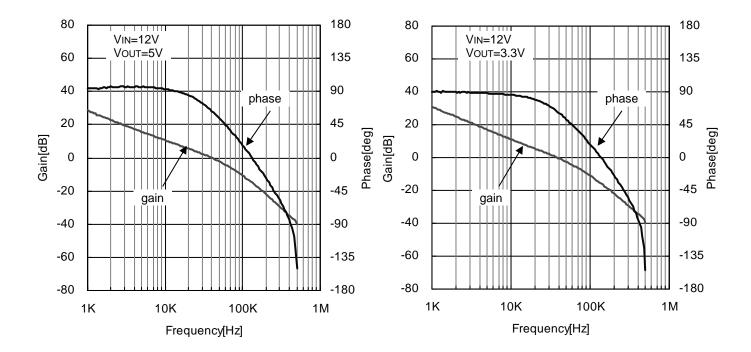
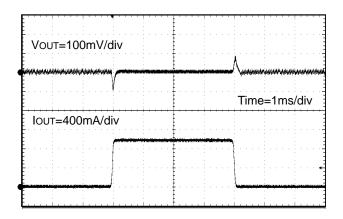


Figure 38. Loop Response Iout=1A (VIN=12V, VOUT=5V, $COUT=Ceramic10\mu F \times 3$)

Figure 39. Loop Response Iout=1A (VIN=12V, VOUT=3.3V, $COUT=Ceramic10\mu F \times 3$)



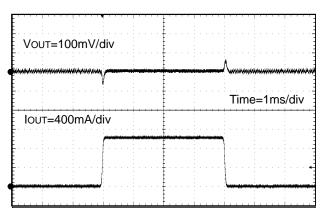


Figure 40. Load Transient Response Iout=10mA - 1A (VIN=12V, Vout=5V, Cout=Ceramic10µF × 3)

Figure 41. Load Transient Response Iout=10mA - 1A (VIN=12V, Vout=3.3V, Cout=Ceramic10µF × 3)

Function Description

1) DC/DC converter operation

BD9E102FJ is a synchronous rectifying step-down switching regulator that achieves faster transient response by employing current mode PWM control system. It utilizes switching operation in PWM (Pulse Width Modulation) mode for heavier load, while it utilizes SLLM (Simple Light Load Mode) control for lighter load to improve efficiency.

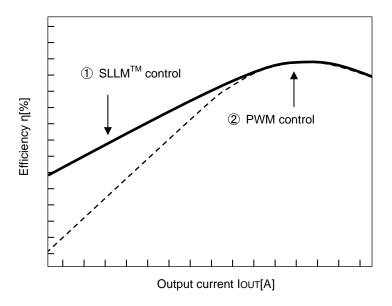


Figure 42. Efficiency (SLLMTM control and PWM control)

①SLLM[™] control

Vout =50mV/div Time=5µs/div SW=5V/div

Figure 43. SW Waveform (①SLLMTM control) (VIN = 12V, VOUT = 5.0V, IOUT = 50mA)

2PWM control

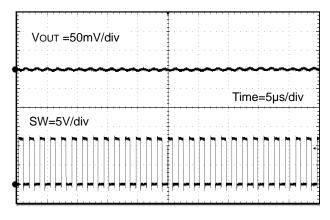


Figure 44. SW Waveform (②PWM control) (VIN = 12V, VOUT = 5.0V, IOUT = 1A)

2) Enable Control

The IC shutdown can be controlled by the voltage applied to the EN terminal. When EN voltage reaches 2.0 V (typ.), the internal circuit is activated and the IC starts up. To enable shutdown control with the EN terminal, set the shutdown interval (Low level interval of EN) must be set to $100 \mu s$ or longer.

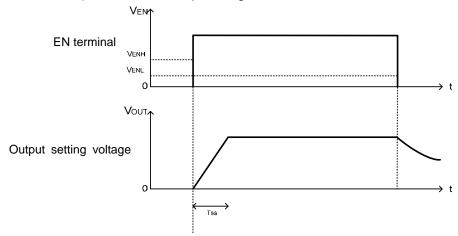


Figure 45. Timing Chart with Enable Control

3) Protective Functions

The protective circuits are intended for prevention of damage caused by unexpected accidents. Do not use them for continuous protective operation.

3-1) Short Circuit Protection (SCP)

The short circuit protection block compares the FB terminal voltage with the internal reference voltage VREF. When the FB terminal voltage has fallen below 0.56 V (typ.) and remained there for 0.9 msec (typ.), SCP stops the operation for 14.4 msec (typ.) and subsequently initiates a restart.

Table 1. Short circuit protection function

| EN pin | FB pin | Short circuit protection | Short circuit protection operation | |
|-----------------|-----------------|--------------------------|------------------------------------|--|
| 20 V or higher | < 0.56 V (typ.) | Enabled | ON | |
| 2.0 V or higher | > 0.56 V (typ.) | Enabled | OFF | |
| 0.8 V or lower | - | Disabled | OFF | |

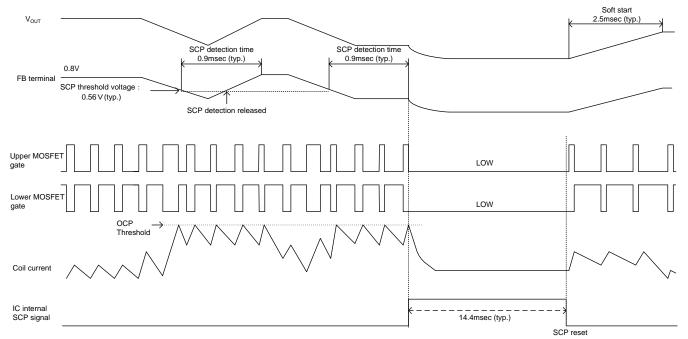


Figure 46. Short circuit protection function (SCP) timing chart

3-2) Under Voltage Lockout Protection (UVLO)

The under voltage lockout protection circuit monitors the VIN terminal voltage.

The operation enters standby when the VIN terminal voltage is 6.4 V (typ.) or lower.

The operation starts when the VIN terminal voltage is 6.6 V (typ.) or higher.

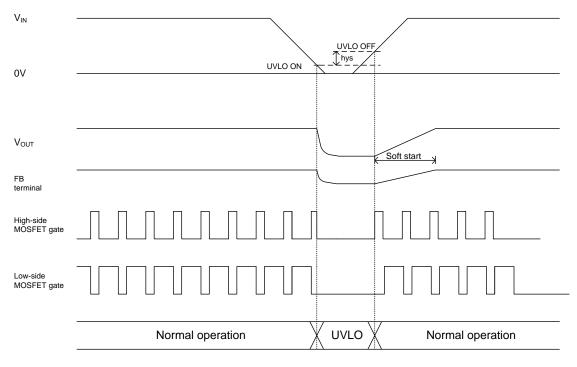


Figure 47. UVLO Timing Chart

3-3) Thermal Shutdown Function (TSD)

When the chip temperature exceeds $Tj = 175^{\circ}C$, the DC/DC converter output is stopped. The thermal shutdown circuit is intended for shutting down the IC from thermal runaway in an abnormal state with the temperature exceeding $Tjmax = 150^{\circ}C$. It is not meant to protect or guarantee the soundness of the application. Do not use the function of this circuit for application protection design.

3-4) Over Current Protection Function (OCP)

The overcurrent protection function is realized by using the current mode control to limit the current that flows through the high-side MOSFET at each cycle of the switching frequency.

3-5) Over Voltage Protection Function (OVP)

Over voltage protection function (OVP) compares FB terminal voltage with internal standard voltage VREF and when FB terminal voltage exceeds1.04V (typ) it turns MOSFET of output part MOSFET OFF. After output voltage drop it returns with hysteresis.

Application Example

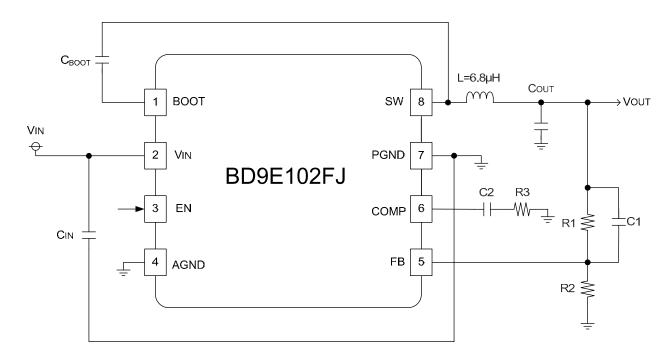


Figure 48. Application Circuit

Table 2. Recommendation Circuit constants

| Vin | 12V | | | | | |
|-------|-------------------|-------------------|---------------------------------|-------------------|-------------------|---------------------------------|
| Vout | 5V | | | | 3.3V | |
| CIN | 10μF | 10μF | 10µF | 10μF | 10µF | 10µF |
| Своот | 0.1µF | 0.1µF | 0.1µF | 0.1µF | 0.1µF | 0.1µF |
| L | 6.8µH | 6.8µH | 6.8µH | 6.8µH | 6.8µH | 6.8µH |
| R1 | 430kΩ | 430kΩ | 430kΩ | 470kΩ | 470kΩ | 470kΩ |
| R2 | 82kΩ | 82kΩ | 82kΩ | 150kΩ | 150kΩ | 150kΩ |
| R3 | 91kΩ | 82kΩ | 51kΩ | 68kΩ | 56kΩ | 43kΩ |
| C1 | - | 13pF | 10pF | - | 13pF | 10pF |
| C2 | 680pF | 360pF | 100pF | 1200pF | 470pF | 160pF |
| Соит | Ceramic 22µFx3 | Ceramic 10µFx3 | Ceramic 10µF and Aluminum | Ceramic 22µFx3 | Ceramic 10µFx3 | Ceramic 10µF and Aluminum |
| 1 | | | 100µF | | | 100µF |

Selection of Components Externally Connected

1) Output LC Filter

The DC/DC converter requires an LC filter for smoothing the output voltage in order to supply a continuous current to the load. BD9E102FJ is returned to the IC and IL ripple current flowing through the inductor for SLLMTM control. This feedback current, Inductance value is the behavior of the best when the 6.8μH. Therefore, the inductor to use is recommended 6.8μH.

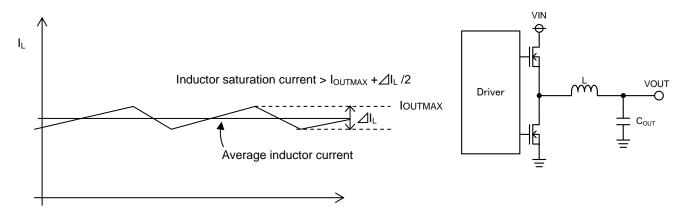


Figure 49. Waveform of current through inductor

Figure 50. Output LC filter circuit

Computation with VIN = 12V, VOUT = 5V, L=6.8µH, switching frequency Fosc= 570kHz, the method is as below.

Inductor ripple current

$$\triangle$$
IL = VOUT × (VIN - VOUT) × $\frac{1}{\text{VIN} \times \text{FOSC} \times \text{L}}$ = 752 mA

Also for saturation current of inductor, select the one with larger current than maximum output current added by 1/2 of inductor ripple current ΔI L.

Output capacitor Cout affects output ripple voltage characteristics. Select output capacitor Cout so that necessary ripple voltage characteristics are satisfied.

Output ripple voltage can be expressed in the following method.

$$\Delta V_{RPL} = \Delta I_{L} \times (RESR + \frac{1}{8 \times COUT \times FOSC}) V$$

RESR is the serial equivalent series resistance here.

With Cout = 66μ F, Resr = $10m\Omega$ the output ripple voltage is calculated as

$$\Delta V \text{RPL} = 0.75 \times (10\text{m} + 1 / (8 \times 66\mu \times 570\text{k})) = 10\text{mV}$$

*Be careful of total capacitance value, when additional capacitor CLOAD is connected in addition to output capacitor COUT. Use maximum additional capacitor CLOAD(max.) condition which satisfies the following method.

Maximum starting inductor ripple current lLSTART < Over Current limit 1.9A (min.)

Maximum starting inductor ripple current lustart can be expressed in the following method.

ILSTART = Maximum starting output current (IOMAX) + Charge current to output capacitor(ICAP) + $\frac{\Delta IL}{2}$

Charge current to output capacitor ICAP can be expressed in the following method.

$$ICAP = \frac{(COUT + CLOAD) \times VOUT}{TSS} A$$

Computation with VIN = 12V, VOUT = 5V, L = 6.8μ H, IOMAX = 1A (max.), switching frequency FOSC= 484kHz (min.), Output capacitor COUT = 66μ F, Soft Start time Tss = 1.2ms (min.), the method is as below.

CLOAD (max.)
$$< \frac{(1.9 - IOMAX - \Delta IL/2) \times TSS}{VOUT} - COUT = 43.6 \mu F$$

2) Output Voltage Set Point

The output voltage value can be set by the feedback resistance ratio.

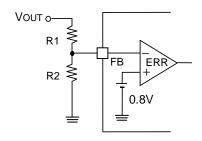


Figure 51. Feedback resister circuit

$$VouT = \frac{R1 + R2}{R2} \times 0.8 \text{ V}$$

Minimum pulse range that output can output stably through all the load area is 250nsec for BD9E102FJ. Use input/output condition which satisfies the following method.

250 nsec ≤
$$\frac{\text{Vout}}{\text{Vin}}$$
 × 1.75 µsec

3) Phase Compensation

A current mode control buck DC/DC converter is a two-pole, one-zero system: two poles formed by an error amplifier and load and one zero point added by phase compensation. The phase compensation resistor R_{CMP} determines the crossover frequency F_{CRS} where the total loop gain of the DC/DC converter is 0 dB. Specifying a high value for this crossover frequency F_{CRS} provides a good load transient response characteristic but inferior stability. Conversely, specifying a low value for the crossover frequency F_{CRS} greatly stabilizes the characteristics but the load transient response characteristic is impaired.

3-1) Selection of Phase Compensation Resistor R_{CMP}

The phase compensation resistance R_{CMP} can be determined by using the following equation.

$$RCMP = \frac{2\pi \times Vout \times FCRS \times COUT}{VFB \times GMP \times GMA} \Omega$$

V_{OUT}: output voltage

 F_{CRS} : crossover frequency C_{OUT} : output capacitanceor

V_{FB}: feedback reference voltage (0.8 V (typ.))

G_{MP}: current sense gain (7 A/V (typ.))

 G_{MA} : error amplifier transconductance (82 $\mu A/V$ (typ.))

3-2) Selection of phase compensation capacitance C_{CMP}

For stable operation of the DC/DC converter, inserting a zero point at 1/6 of the zero crossover frequency that cancels the phase delay due to the pole formed by the load often provides favorable characteristics.

The phase compensation capacitance C_{CMP} can be determined by using the following equation.

$$C_{CMP} = \frac{1}{2\pi \times R_{CMP} \times F_Z} F$$

Fz: Zero point inserted

3-3) Loop stability

To ensure the stability of the DC/DC converter, use the actual device to make sure that a sufficient phase margin is provided. Ensuring a phase margin of at least 45 degrees in the worst conditions is recommended. The feed forward capacitor C_{RUP} is used for the purpose of forming a zero point together with the resistor R_{UP} to increase the phase margin within the limited frequency range. Using a C_{RUP} is effective when the R_{UP} resistance is larger than the combined parallel resistance of R_{UP} and R_{DW} .

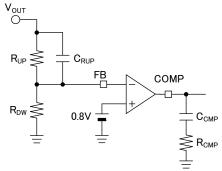


Figure 52. Phase compensation circuit

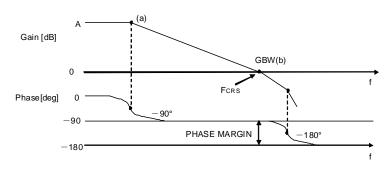


Figure 53. Bode plot

PCB Layout Design

In the buck DC/DC converter, a large pulsed current flows in two loops. The first loop is the one into which the current flows when the High Side FET is turned on. The flow starts from the input capacitor C_{IN} , runs through the FET, inductor L and output capacitor C_{OUT} and back to ground of C_{IN} via ground of C_{OUT} . The second loop is the one into which the current flows when the Low Side FET is turned on. The flow starts from the Low Side FET, runs through the inductor L and output capacitor C_{OUT} and back to ground of the Low Side FET via ground of C_{OUT} . Tracing these two loops as thick and short as possible allows noise to be reduced for improved efficiency. It is recommended to connect the input and output capacitors, in particular, to the ground plane. The PCB layout has a great influence on the DC/DC converter in terms of all of the heat generation, noise and efficiency characteristics.

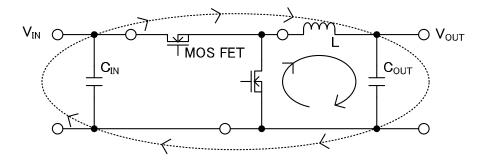
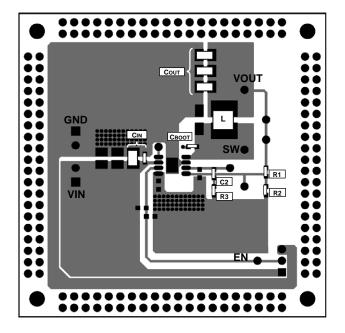
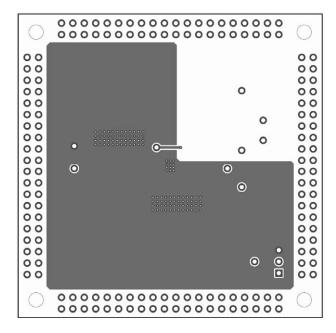


Figure 54. Current loop of buck converter

Accordingly, design the PCB layout with particular attention paid to the following points.

- Provide the input capacitor as close to the IC VIN terminal as possible on the same plane as the IC.
- If there is any unused area on the PCB, provide a copper foil plane for the ground node to assist heat dissipation from the IC and the surrounding components.
- Switching nodes such as SW are susceptible to noise due to AC coupling with other nodes. Trace to the coil as thick and as short as possible.
- Provide lines connected to FB and COMP as far away from the SW node.
- Provide the output capacitor away from the input capacitor in order to avoid the effect of harmonic noise from the input.





Top Layer Bottom Layer

Figure 55. Example of sample board layout pattern

Power Dissipation

When designing the PCB layout and peripheral circuitry, sufficient consideration must be given to ensure that the power dissipation is within the allowable dissipation curve.

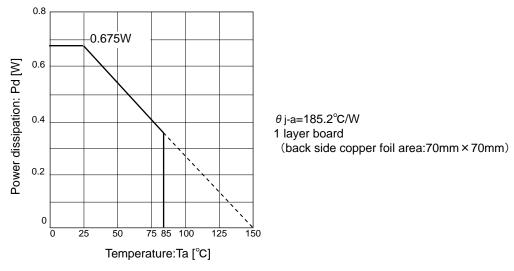


Figure 56. Power dissipation (SOP-J8)

● I/O Equivalence Circuit

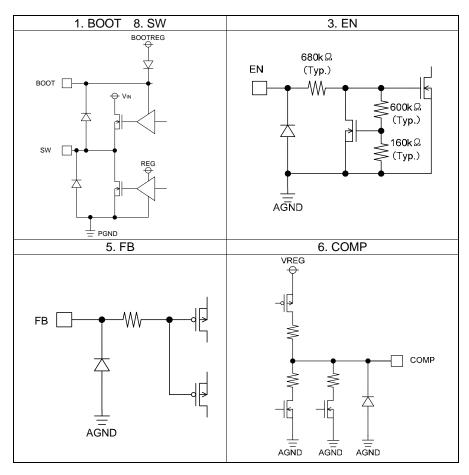


Figure 57. I/O equivalence circuit

Operational Notes

1) Absolute Maximum Ratings

While abundant attention is paid to quality management of this IC, use of the IC in excess of absolute maximum ratings such as the applied voltage and operating temperature range may result in deterioration or damage. For design, ensure that it is always used within the guaranteed range. Use of the IC in excess of absolute maximum ratings such as the applied voltage and operating temperature range may result in damage. The state of the IC (short mode, open mode, etc.) cannot be identified if such damage occurs. Physical safety measures such as provision of a fuse should be taken when a special mode in which the absolute maximum ratings may be exceeded is anticipated.

2) GND Potential

Ensure the minimum GND pin potential in all operating conditions.

3) Thermal Design

Use a thermal design that allows for a sufficient margin in light of the power dissipation (Pd) in actual operating conditions.

4) Pin Short and Faulty Mounting

Use caution when orienting and positioning the IC for mounting on printed circuit boards. Improper mounting may result in damage to the IC. Avoid short-circuiting between VIN and Vout/SW. Short-circuiting between these may result in damage to the IC and smoke generation. In a case that has been applied VIN = 20V or more, when there is a possibility the BOOT terminal and SW terminal is short-circuited, please insert a resistance of about 10 ohms between the bootstrap capacitor $0.1\mu F$ and BOOT terminal. Short-circuiting between these without inserting this resistance may result in damage to the IC and smoke generation.

5) Actions is Strong Magnetic Field

Use caution when using the IC in the presence of a strong magnetic field as doing so may cause the IC to malfunction.

6) Testing on Application Boards

When testing the IC on an application board, connecting a capacitor to a pin with a low impedance may subject the IC to stress. Always discharge capacitors after each process. Always turn the power supply off before connecting it to or removing it from a jig or fixture during the inspection process. As an antistatic measure, ground the IC during assembly steps and use similar caution when transporting or storage the IC.

7) PCB Layout

Be sure to connect VIN to the power supply on the board.

Be sure to connect PGND and AGND to the GND on the board.

Ensure that the VIN wiring is thick and short for a sufficiently low impedance.

Ensure that the PGND and AGND wiring is thick and short for a sufficiently low impedance.

Take the output voltage of the DC/DC converter from the two ends of the output capacitor.

The PCB layout and peripheral components may influence the performance of the DC/DC converter. Give sufficient consideration to the design of the peripheral circuitry.

8) IC Pin Input

This IC is a monolithic IC and, between each element, it has P+ isolation for element separation and P substrate. With this P layer and the N layer of the respective elements, P-N junctions are formed to constitute a variety of parasitic elements. For example, when a resistor and transistor are connected to terminals as shown in the figure below, reversal of the terminal voltage and GND voltage activates the parasitic diode and transistor.

Parasitic elements are inevitably generated by the potential relationship due to the IC structure. Activation of a parasitic element may cause interference in circuit operation, possibly leading to damage. Accordingly, use abundance of caution to avoid use that causes the parasitic elements to operate such as applying a voltage that is lower than the GND (P substrate) to an I/O terminal.

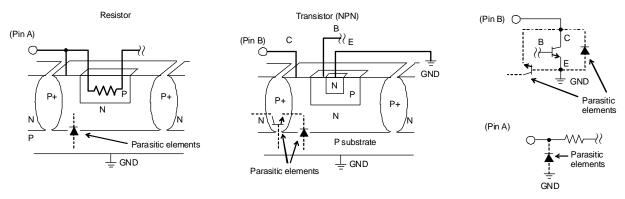


Figure 58. Example of simplified structure of monolithic IC

9) Overcurrent protection Circuit

The DC/DC converter output terminal integrates an overcurrent protection function, which is effective in protecting the IC from damage caused by unexpected GND short circuit. Avoid use on the premise of continuous operation of the protection circuit.

10) Thermal Shutdown Circuit

If the chip temperature reaches Tj = 175°C (typ.), the thermal shutdown function is activated and the DC/DC converter stops switching.

The thermal shutdown circuit is intended for shutting down the IC from thermal runaway and is not meant to protect or guarantee the soundness of the application. Accordingly, avoid use on the premise of continuous use or operation after the activation of this circuit.

11) Enable Function

If the rate of fall of the EN terminal signal is too low, chattering may occur. Chattering with the output voltage remaining may generate a reverse current that boosts the voltage from the output to the input, possibly leading to damage. For on/off control with the EN signal, ensure that the signal falls within 100 µsec.

12) Load at Startup

Ensure that the respective output has light load at startup of this IC.

Restrain the power supply line noise at startup and voltage drop generated by operating current within the hysteresis width of UVLO. Input of any noise exceeding the hysteresis noise width may cause malfunction.

13) External Elements

Use a ceramic capacitor with a low ESR for the bypass capacitor between VIN and PGND and provide it as close to the IC as possible. For external components such as inductors and capacitors, use theose recommended in this specification and provide as close to the IC as possible. For those through which large current flows, in particular, ensure that the wiring is thick and short.

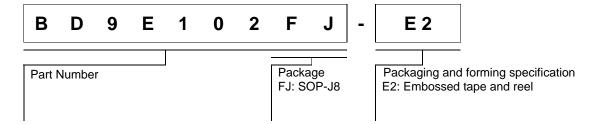
14) IC Applications

This IC is not developed for in-vehicle or military applications or equipment/devices that may affect human lives. Do not use the IC for such applications. If this IC is used by customers in any of such applications as described above, ROHM shall not be held responsible for failure to satisfy the requirements concerned.

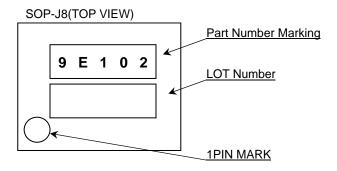
15) Use Environment

The operating temperature range is intended to guarantee functional operation and does not guarantee the life of the IC within this range. The life of the IC may be subject to derating depending on use environment such as the voltage applied, ambient temperature and humidity. Design equipment and devices in view of derating.

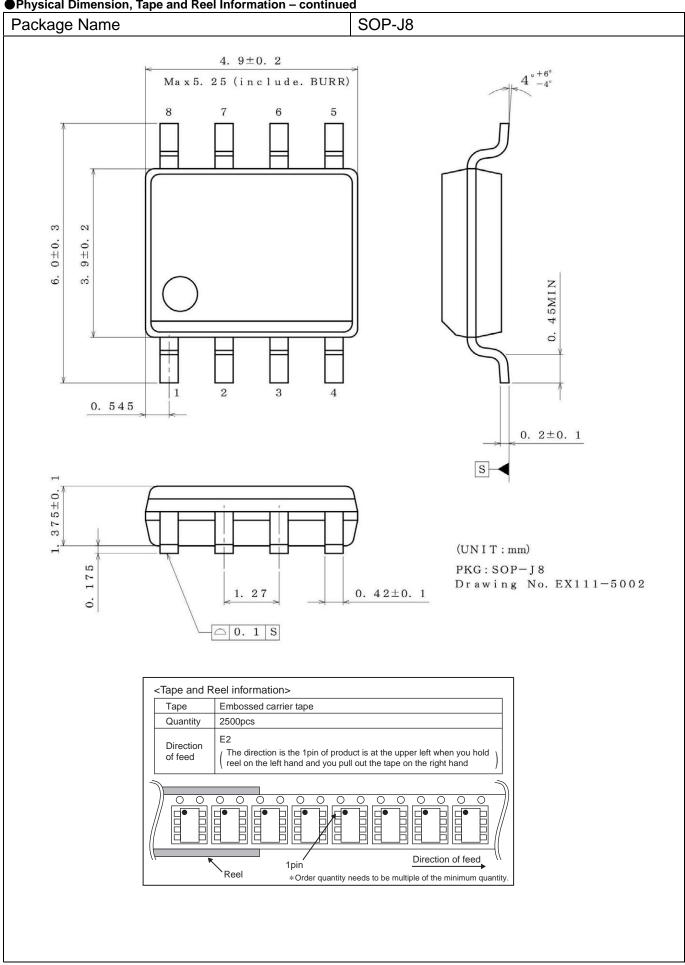
Ordering Information



Marking Diagram



●Physical Dimension, Tape and Reel Information – continued



Revision History

| Date | Revision | Description |
|-------------|----------|-------------|
| 1. May. '13 | 001 | Created |

Notice

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| JAPAN | USA | EU | CHINA | |
|---------|----------|------------|----------|--|
| CLASSⅢ | CL ACCTI | CLASS II b | CLASSIII | |
| CLASSIV | CLASSⅢ | CLASSⅢ | CLASSⅢ | |

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 - [b] Installation of redundant circuits to reduce the impact of single or multiple circuit failure
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 - [b] Use of our Products outdoors or in places where the Products are exposed to direct sunlight or dust
 - [c] Use of our Products in places where the Products are exposed to sea wind or corrosive gases, including Cl₂, H₂S, NH₃, SO₂, and NO₂
 - [d] Use of our Products in places where the Products are exposed to static electricity or electromagnetic waves
 - [e] Use of our Products in proximity to heat-producing components, plastic cords, or other flammable items
 - [f] Sealing or coating our Products with resin or other coating materials
 - [g] Use of our Products without cleaning residue of flux (even if you use no-clean type fluxes, cleaning residue of flux is recommended); or Washing our Products by using water or water-soluble cleaning agents for cleaning residue after soldering
 - [h] Use of the Products in places subject to dew condensation
- 4. The Products are not subject to radiation-proof design.
- 5. Please verify and confirm characteristics of the final or mounted products in using the Products.
- 6. In particular, if a transient load (a large amount of load applied in a short period of time, such as pulse. is applied, confirmation of performance characteristics after on-board mounting is strongly recommended. Avoid applying power exceeding normal rated power; exceeding the power rating under steady-state loading condition may negatively affect product performance and reliability.
- 7. De-rate Power Dissipation (Pd) depending on Ambient temperature (Ta). When used in sealed area, confirm the actual ambient temperature.
- 8. Confirm that operation temperature is within the specified range described in the product specification.
- 9. ROHM shall not be in any way responsible or liable for failure induced under deviant condition from what is defined in this document.

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- 1. When a highly active halogenous (chlorine, bromine, etc.) flux is used, the residue of flux may negatively affect product performance and reliability.
- 2. In principle, the reflow soldering method must be used; if flow soldering method is preferred, please consult with the ROHM representative in advance.

For details, please refer to ROHM Mounting specification

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- Use Products within the specified time after opening a humidity barrier bag. Baking is required before using Products of which storage time is exceeding the recommended storage time period.

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