

## OPA4188 0.03 $\mu\text{V}/^\circ\text{C}$ 漂移、低噪声、轨到轨输出、36V、零漂移运算放大器

### 1 特性

- 低偏移电压: 25 $\mu\text{V}$  (最大值)
- 零漂移: 0.03 $\mu\text{V}/^\circ\text{C}$
- 低噪声: 8.8 nV/ $\sqrt{\text{Hz}}$   
0.1Hz 至 10Hz 噪声: 0.25 $\mu\text{V}_{\text{PP}}$
- 出色的直流精度:  
电源抑制比 (PSRR): 142dB  
共模抑制比 (CMRR): 146dB  
开环路增益: 136dB
- 增益带宽: 2MHz
- 静态电流: 475 $\mu\text{A}$  (最大值)
- 宽电源电压:  $\pm 2\text{V}$  至  $\pm 18\text{V}$
- 轨到轨输出:  
输入包括负电源轨
- 已过滤射频干扰 (RFI) 的输入
- 微型尺寸封装

### 2 应用范围

- 桥式放大器
- 应力计
- 测试设备
- 传感器 应用
- 温度测量
- 电子称
- 医疗仪表
- 电阻式温度检测器
- 精密有源滤波器

### 3 说明

OPA4188 运算放大器采用 TI 专有的自动归零技术，可在时间和温度范围内提供低偏移电压 (25 $\mu\text{V}$ ，最大值) 以及近似为零的漂移。此类微型、高精度、低静态电流放大器提供高输入阻抗以及不超过

15mV 电源轨电压的轨到轨输出摆幅，非常适用于工业集成电机驱动器解决方案。输入共模范围包括负电源轨。单电源或双电源可在 4V 至 36V ( $\pm 2\text{V}$  至  $\pm 18\text{V}$ ) 范围内使用。

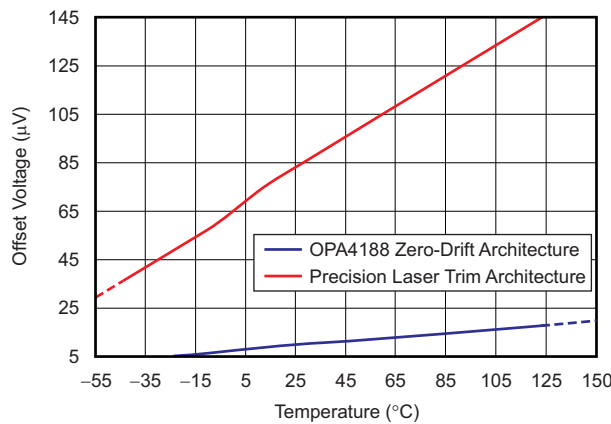
该器件的四路版本采用 14 引脚小外形尺寸集成电路 (SOIC) 封装和 14 引脚薄型小外形尺寸 (TSSOP) 封装。所有器件版本的额定工作温度范围均为  $-40^\circ\text{C}$  至  $+125^\circ\text{C}$ 。

#### 器件信息<sup>(1)</sup>

器件型号	封装	封装尺寸 (标称值)
OPA4188	SOIC (14)	8.65mm x 3.91mm
	TSSOP (14)	5.00mm x 4.40mm

(1) 要了解所有可用封装，请见数据表末尾的可订购产品附录。

零漂移架构提升性能



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## 4 修订历史记录

注：之前版本的页码可能与当前版本有所不同。

<b>Changes from Revision C (April 2015) to Revision D</b>	<b>Page</b>
• Changed high supply over-temperature input bias current limit in <i>High-Voltage Operation Electrical Characteristics</i> table .....	6
• Changed high supply noise units in <i>High-Operating Voltage Electrical Characteristics</i> table .....	6
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• Changed high supply over-temperature quiescent current limit in <i>High-Voltage Operation Electrical Characteristics</i> table .....	7
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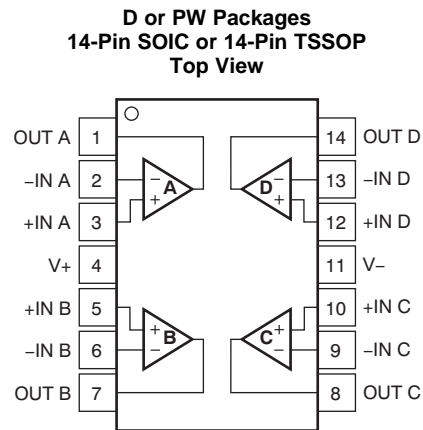
<b>Changes from Revision A (September 2012) to Revision B</b>	<b>Page</b>
• Changed maximum specification of second Input Bias Current, $I_B$ parameter row in <i>High-Voltage Operation Electrical Characteristics</i> table .....	6
• Changed maximum specification of second <i>Input Bias Current</i> ( $I_B$ ) parameter in <i>Low-Voltage Electrical Characteristics</i> table .....	7
• Changed typical specifications for <i>Input impedance (Common-mode)</i> parameter in <i>Low-Voltage Electrical Characteristics</i> table .....	7

<b>Changes from Original (June 2012) to Revision A</b>	<b>Page</b>
• 已更改 第二个至最后一个应用要点 .....	1

## 5 Zero-Drift Amplifier Portfolio

VERSION	PRODUCT	OFFSET VOLTAGE ( $\mu\text{V}$ )	OFFSET VOLTAGE DRIFT ( $\mu\text{V}/^\circ\text{C}$ )	BANDWIDTH (MHz)
Single	<a href="#">OPA188</a> (4 V to 36 V)	25	0.085	2
	<a href="#">OPA333</a> (5 V)	10	0.05	0.35
	<a href="#">OPA378</a> (5 V)	50	0.25	0.9
	<a href="#">OPA735</a> (12 V)	5	0.05	1.6
Dual	<a href="#">OPA2188</a> (4 V to 36 V)	25	0.085	2
	<a href="#">OPA2333</a> (5 V)	10	0.05	0.35
	<a href="#">OPA2378</a> (5 V)	50	0.25	0.9
	<a href="#">OPA2735</a> (12 V)	5	0.05	1.6
Quad	<a href="#">OPA4188</a> (4 V to 36 V)	25	0.085	2
	<a href="#">OPA4330</a> (5 V)	50	0.25	0.35

## 6 Pin Configuration and Functions



### Pin Functions

PIN		I/O	DESCRIPTION
NO.	NAME		
1	OUT A	O	Output channel A
2	-IN A	I	Inverting input channel A
3	+IN A	I	Noninverting input channel A
4	V+	I	Positive power supply
5	+IN B	I	Noninverting input channel B
6	-IN B	I	Inverting input channel B
7	OUT B	O	Output channel B
8	OUT C	O	Output channel C
9	-IN C	I	Inverting input channel C
10	+IN C	I	Noninverting input channel C
11	V-	I	Negative power supply
12	+IN D	I	Noninverting input channel D
13	-IN D	I	Inverting input channel D
14	OUT D	O	Output channel D

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Supply voltage		±20	40 (single supply)	V
Signal input terminals <sup>(2)</sup>	Voltage	(V <sub>-</sub> ) – 0.5	(V <sub>+</sub> ) + 0.5	V
	Current	±10		mA
Output short circuit <sup>(3)</sup>		Continuous		
Temperature	Operating, T <sub>A</sub>	–55	150	°C
	Junction, T <sub>J</sub>	150		°C
	Storage, T <sub>stg</sub>	–65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5-V beyond the supply rails should be current-limited to 10 mA or less.
- (3) Short-circuit to ground, one amplifier per package.

### 7.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins <sup>(1)</sup>	±2000
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins <sup>(2)</sup>	±1000

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	NOM	MAX	UNIT
Power supply voltage, (V <sub>+</sub> )-(V <sub>-</sub> )	4 (±2)		36 (±18)	V
Ambient temperature, T <sub>A</sub>	–40		125	°C

### 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		OPA4188		UNIT
		D (SOIC)	PW (TSSOP)	
		14 PINS	14 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	93.2	106.9	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	51.8	24.4	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	49.4	59.3	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	13.5	0.6	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	42.2	54.3	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	N/A	°C/W

- (1) For more information about traditional and new thermal metrics, see [Semiconductor and IC Package Thermal Metrics](#) (SPRA953).

### 7.5 Electrical Characteristics: High-Voltage Operation, $V_S = \pm 4\text{ V}$ to $\pm 18\text{ V}$ ( $V_S = 8\text{ V}$ to $36\text{ V}$ )

at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $V_{\text{COM}} = V_{\text{OUT}} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>						
$V_{\text{OS}}$	Input offset voltage	$T_A = 25^\circ\text{C}$		6	25	$\mu\text{V}$
$dV_{\text{OS}}/dT$		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		0.03	0.085	$\mu\text{V}/^\circ\text{C}$
PSRR	Power-supply rejection ratio	$V_S = 4\text{ V}$ to $36\text{ V}$ , $V_{\text{CM}} = V_S / 2$		0.075	0.3	$\mu\text{V}/\text{V}$
		$V_S = 4\text{ V}$ to $36\text{ V}$ , $V_{\text{CM}} = V_S / 2$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			0.3	$\mu\text{V}/\text{V}$
	Long-term stability			4 <sup>(1)</sup>		$\mu\text{V}$
	Channel separation, DC			1		$\mu\text{V}/\text{V}$
<b>INPUT BIAS CURRENT</b>						
$I_B$	Input bias current	$V_{\text{CM}} = V_S / 2$		$\pm 160$	$\pm 1400$	$\text{pA}$
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 18$	$\text{nA}$
$I_{\text{OS}}$	Input offset current			$\pm 320$	$\pm 2800$	$\text{pA}$
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 6$	$\text{nA}$
<b>NOISE</b>						
$e_n$	Input voltage noise	$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		0.25		$\mu\text{V}_{\text{PP}}$
$e_n$	Input voltage noise density	$f = 1\text{ kHz}$		8.8		$\text{nV}/\sqrt{\text{Hz}}$
$i_n$	Input current noise density	$f = 1\text{ kHz}$		7		$\text{fA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>						
$V_{\text{CM}}$	Common-mode voltage range	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	$V^-$		$(V^+) - 1.5$	$\text{V}$
CMRR	Common-mode rejection ratio	$(V^-) < V_{\text{CM}} < (V^+) - 1.5\text{ V}$	120	134		$\text{dB}$
		$(V^-) + 0.5\text{ V} < V_{\text{CM}} < (V^+) - 1.5\text{ V}$ , $V_S = \pm 18\text{ V}$	130	146		$\text{dB}$
		$(V^-) + 0.5\text{ V} < V_{\text{CM}} < (V^+) - 1.5\text{ V}$ , $V_S = \pm 18\text{ V}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	120	126		$\text{dB}$
<b>INPUT IMPEDANCE</b>						
Input impedance	Differential			$100 \parallel 6$		$\text{M}\Omega \parallel \text{pF}$
	Common-mode			$6 \parallel 9.5$		$10^{12}\ \Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>						
$A_{\text{OL}}$	Open-loop voltage gain	$(V^-) + 500\text{ mV} < V_O < (V^+) - 500\text{ mV}$ , $R_L = 10\text{ k}\Omega$	130	136		$\text{dB}$
		$(V^-) + 500\text{ mV} < V_O < (V^+) - 500\text{ mV}$ , $R_L = 10\text{ k}\Omega$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	118	126		$\text{dB}$
<b>FREQUENCY RESPONSE</b>						
GBW	Gain-bandwidth product			2		$\text{MHz}$
SR	Slew rate	$G = 1$		0.8		$\text{V}/\mu\text{s}$
$t_s$	Settling time	0.1%	$V_S = \pm 18\text{ V}$ , $G = 1$ , 10-V step	20		$\mu\text{s}$
		0.01%	$V_S = \pm 18\text{ V}$ , $G = 1$ , 10-V step	27		$\mu\text{s}$
	Overload recovery time	$V_{\text{IN}} \times G = V_S$		1		$\mu\text{s}$
THD+N	Total harmonic distortion + noise	1 kHz, $G = 1$ , $V_{\text{OUT}} = 1\text{ V}_{\text{RMS}}$		0.0001%		

(1) 1000-hour life test at  $+125^\circ\text{C}$  demonstrated randomly distributed variation in the range of measurement limits—approximately  $4\ \mu\text{V}$ .

## Electrical Characteristics: High-Voltage Operation, $V_S = \pm 4\text{ V}$ to $\pm 18\text{ V}$ ( $V_S = 8\text{ V}$ to $36\text{ V}$ ) (continued)

at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $V_{\text{COM}} = V_{\text{OUT}} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OUTPUT</b>						
Voltage output swing from rail	No load			6	15	mV
	$R_L = 10\text{ k}\Omega$			220	250	mV
	$R_L = 10\text{ k}\Omega$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			310	350	mV
$I_{\text{SC}}$	Short circuit current		$\pm 18$			mA
$R_O$	Open-loop output resistance	$f = 1\text{ MHz}$ , $I_O = 0$		120		$\Omega$
$C_{\text{LOAD}}$	Capacitive load drive			1		nF
<b>POWER SUPPLY</b>						
$V_S$	Operating voltage range		4 to 36 ( $\pm 2$ to $\pm 18$ )			V
$I_Q$	Quiescent current (per amplifier)	$V_S = \pm 4\text{ V}$ to $V_S = \pm 18\text{ V}$		415	500	$\mu\text{A}$
		$I_O = 0\text{ mA}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			570	$\mu\text{A}$
<b>TEMPERATURE RANGE</b>						
Temperature range	Specified		-40		125	$^\circ\text{C}$
	Operating		-55		150	$^\circ\text{C}$
	Storage		-65		150	$^\circ\text{C}$

## 7.6 Electrical Characteristics: Low-Voltage Operation, $V_S = \pm 2\text{ V}$ to $< \pm 4\text{ V}$ ( $V_S = +4\text{ V}$ to $< +8\text{ V}$ )

at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $V_{\text{COM}} = V_{\text{OUT}} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>						
$V_{\text{OS}}$	Input offset voltage	$T_A = 25^\circ\text{C}$		6	25	$\mu\text{V}$
$dV_{\text{OS}}/dT$		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		0.03	0.085	$\mu\text{V}/^\circ\text{C}$
PSRR	Power-supply rejection ratio	$V_S = 4\text{ V}$ to $36\text{ V}$ , $V_{\text{CM}} = V_S / 2$		0.075	0.3	$\mu\text{V}/\text{V}$
		$V_S = 4\text{ V}$ to $36\text{ V}$ , $V_{\text{CM}} = V_S / 2$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			0.3	$\mu\text{V}/\text{V}$
	Long-term stability			4 <sup>(1)</sup>		$\mu\text{V}$
	Channel separation, DC			1		$\mu\text{V}/\text{V}$
<b>INPUT BIAS CURRENT</b>						
$I_B$	Input bias current	$V_{\text{CM}} = V_S / 2$		$\pm 160$	$\pm 1400$	pA
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 18$	nA
$I_{\text{OS}}$	Input offset current			$\pm 320$	$\pm 2800$	pA
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 6$	nA
<b>NOISE</b>						
$e_n$	Input voltage noise	$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		0.25		$\mu\text{V}_{\text{PP}}$
$e_n$	Input voltage noise density	$f = 1\text{ kHz}$		8.8		$\text{nV}/\sqrt{\text{Hz}}$
$i_n$	Input current noise density	$f = 1\text{ kHz}$		7		$\text{fA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>						
$V_{\text{CM}}$	Common-mode voltage range		V-		(V+) - 1.5	V
CMRR	Common-mode rejection ratio	$(V-) < V_{\text{CM}} < (V+) - 1.5\text{ V}$	106	114		dB
		$(V-) + 0.5\text{ V} < V_{\text{CM}} < (V+) - 1.5\text{ V}$ , $V_S = \pm 2\text{ V}$	114	120		dB
		$(V-) + 0.5\text{ V} < V_{\text{CM}} < (V+) - 1.5\text{ V}$ , $V_S = \pm 2\text{ V}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	108	120		dB
<b>INPUT IMPEDANCE</b>						
Input impedance	Differential			100    6		$\text{M}\Omega$    pF
	Common-mode			6    9.5		$10^{12}\ \Omega$    pF

(1) 1000-hour life test at  $+125^\circ\text{C}$  demonstrated randomly distributed variation in the range of measurement limits—approximately  $4\ \mu\text{V}$ .

**Electrical Characteristics: Low-Voltage Operation,  $V_S = \pm 2\text{ V}$  to  $< \pm 4\text{ V}$  ( $V_S = +4\text{ V}$  to  $< +8\text{ V}$ ) (continued)**

 at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $V_{\text{COM}} = V_{\text{OUT}} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OPEN-LOOP GAIN</b>						
$A_{\text{OL}}$	Open-loop voltage gain	$(V^- + 500\text{ mV} < V_O < (V^+ - 500\text{ mV}, R_L = 10\text{ k}\Omega$	120	130		dB
		$(V^- + 500\text{ mV} < V_O < (V^+ - 500\text{ mV}, R_L = 10\text{ k}\Omega, T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	110	120		dB
<b>FREQUENCY RESPONSE</b>						
GBW	Gain-bandwidth product			2		MHz
SR	Slew rate	$G = 1$		0.8		V/ $\mu\text{s}$
	Overload recovery time	$V_{\text{IN}} \times G = V_S$		1		$\mu\text{s}$
THD+N	Total harmonic distortion + noise	1 kHz, $G = 1, V_{\text{OUT}} = 1\text{ V}_{\text{RMS}}$		0.0001%		
<b>OUTPUT</b>						
	Voltage output swing from rail	No load		6	15	mV
		$R_L = 10\text{ k}\Omega$		220	250	mV
		$R_L = 10\text{ k}\Omega, T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		310	350	mV
$I_{\text{SC}}$	Short circuit current			$\pm 18$		mA
$R_O$	Open-loop output resistance	$f = 1\text{ MHz}, I_O = 0$		120		$\Omega$
$C_{\text{LOAD}}$	Capacitive load drive			1		nF
<b>POWER SUPPLY</b>						
$V_S$	Operating voltage range		4 to 36 ( $\pm 2$ to $\pm 18$ )			V
$I_Q$	Quiescent current (per amplifier)	$V_S = \pm 2\text{ V}$ to $V_S = \pm 4\text{ V}$		385	465	$\mu\text{A}$
		$I_O = 0\text{ mA}, T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			540	$\mu\text{A}$
<b>TEMPERATURE RANGE</b>						
Temperature range	Specified		-40		125	$^\circ\text{C}$
	Operating		-40		125	$^\circ\text{C}$
	Storage		-65		150	$^\circ\text{C}$

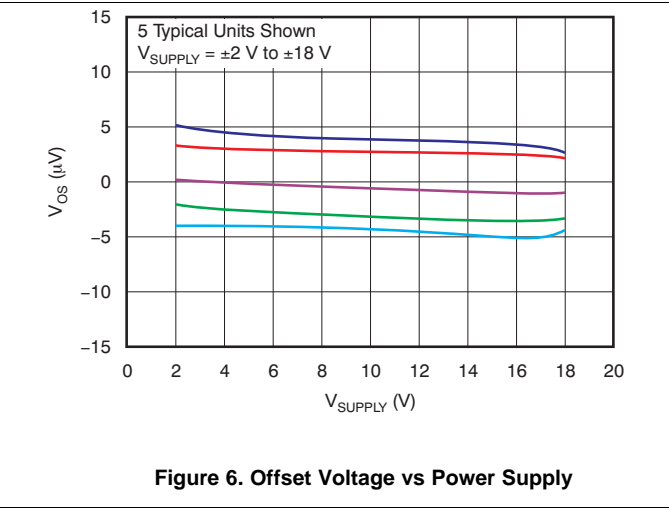
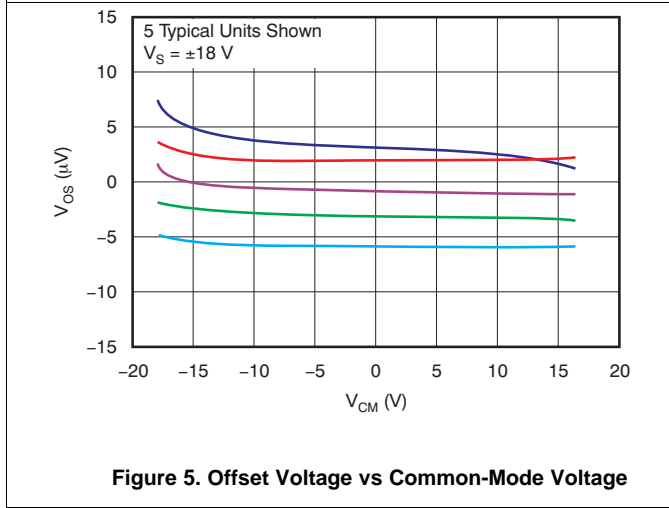
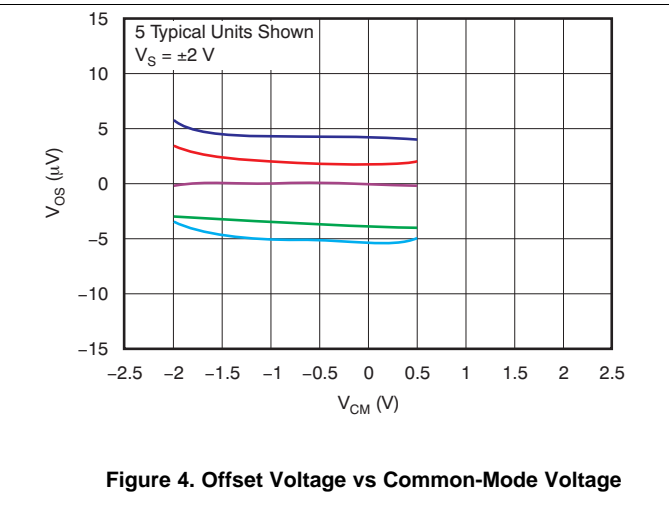
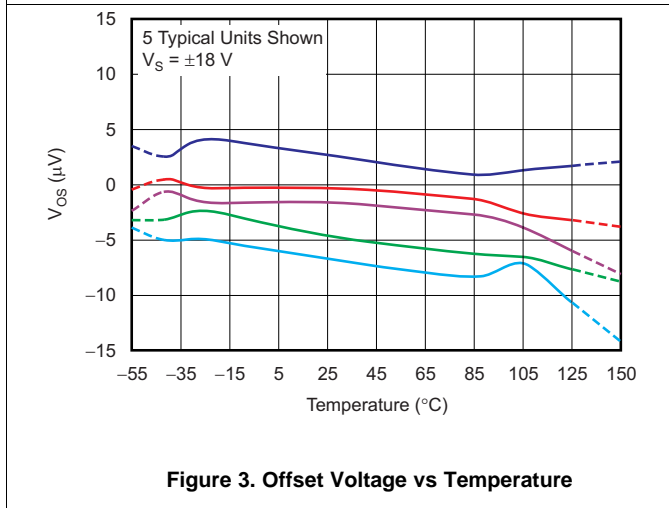
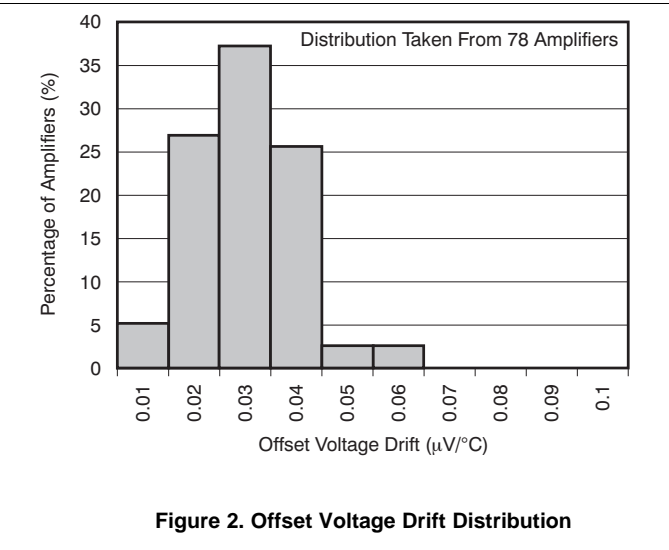
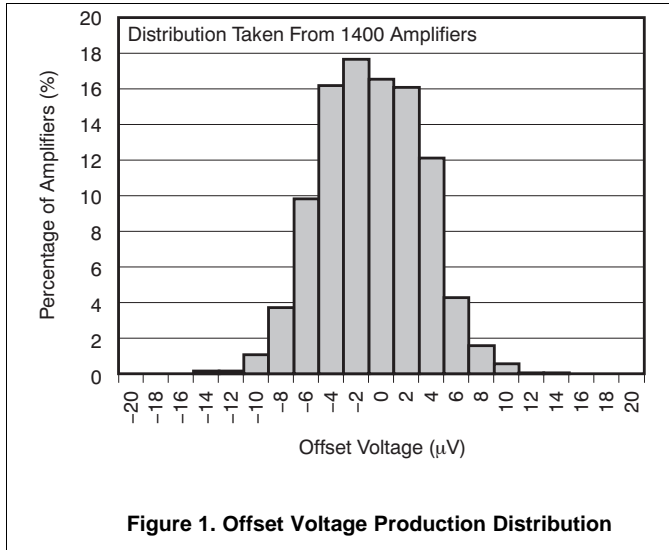


## 7.7 Typical Characteristics

**Table 1. Characteristic Performance Measurements**

DESCRIPTION	FIGURE
Offset Voltage Production Distribution	<a href="#">Figure 1</a>
Offset Voltage Drift Distribution	<a href="#">Figure 2</a>
Offset Voltage vs Temperature	<a href="#">Figure 3</a>
Offset Voltage vs Common-Mode Voltage	<a href="#">Figure 4, Figure 5</a>
Offset Voltage vs Power Supply	<a href="#">Figure 6</a>
$I_B$ and $I_{OS}$ vs Common-Mode Voltage	<a href="#">Figure 7</a>
Input Bias Current vs Temperature	<a href="#">Figure 8</a>
Output Voltage Swing vs Output Current (Maximum Supply)	<a href="#">Figure 9</a>
CMRR and PSRR vs Frequency (Referred-to-Input)	<a href="#">Figure 10</a>
CMRR vs Temperature	<a href="#">Figure 11, Figure 12</a>
PSRR vs Temperature	<a href="#">Figure 13</a>
0.1-Hz to 10-Hz Noise	<a href="#">Figure 14</a>
Input Voltage Noise Spectral Density vs Frequency	<a href="#">Figure 15</a>
THD+N Ratio vs Frequency	<a href="#">Figure 16</a>
THD+N vs Output Amplitude	<a href="#">Figure 17</a>
Quiescent Current vs Supply Voltage	<a href="#">Figure 18</a>
Quiescent Current vs Temperature	<a href="#">Figure 19</a>
Open-Loop Gain and Phase vs Frequency	<a href="#">Figure 20</a>
Closed-Loop Gain vs Frequency	<a href="#">Figure 21</a>
Open-Loop Gain vs Temperature	<a href="#">Figure 22</a>
Open-Loop Output Impedance vs Frequency	<a href="#">Figure 23</a>
Small-Signal Overshoot vs Capacitive Load (100-mV Output Step)	<a href="#">Figure 24, Figure 25</a>
No Phase Reversal	<a href="#">Figure 26</a>
Positive Overload Recovery	<a href="#">Figure 27</a>
Negative Overload Recovery	<a href="#">Figure 28</a>
Small-Signal Step Response (100 mV)	<a href="#">Figure 29, Figure 30</a>
Large-Signal Step Response	<a href="#">Figure 31, Figure 32</a>
Large-Signal Settling Time (10-V Positive Step)	<a href="#">Figure 33</a>
Large-Signal Settling Time (10-V Negative Step)	<a href="#">Figure 34</a>
Short Circuit Current vs Temperature	<a href="#">Figure 35</a>
Maximum Output Voltage vs Frequency	<a href="#">Figure 36</a>
Channel Separation vs Frequency	<a href="#">Figure 37</a>
EMIRR IN+ vs Frequency	<a href="#">Figure 38</a>

$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.



$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.

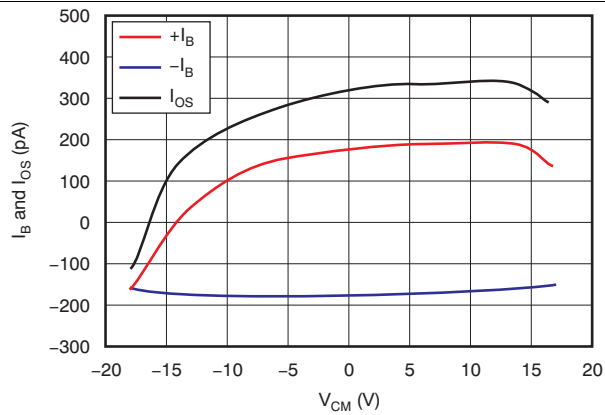


Figure 7.  $I_B$  and  $I_{OS}$  vs Common-Mode Voltage

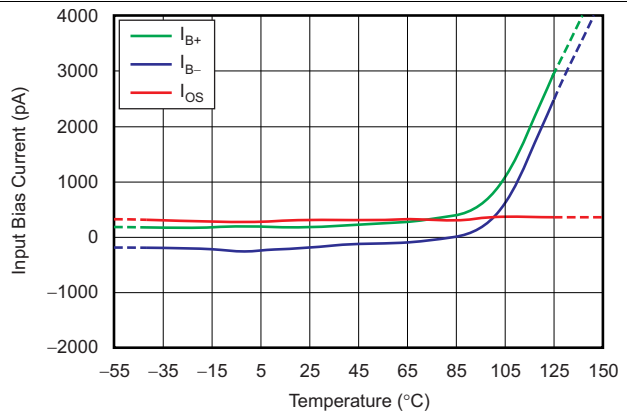


Figure 8. Input Bias Current vs Temperature

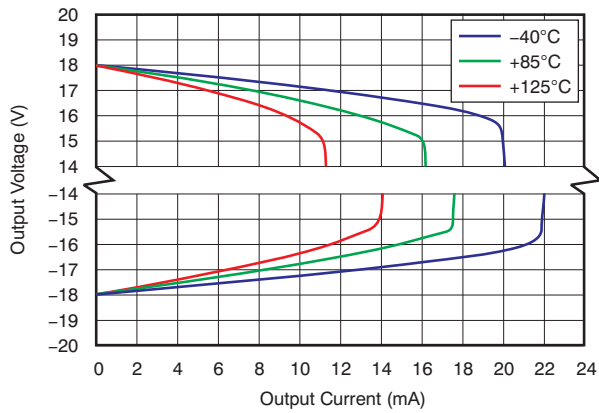


Figure 9. Output Voltage Swing vs Output Current (Maximum Supply)

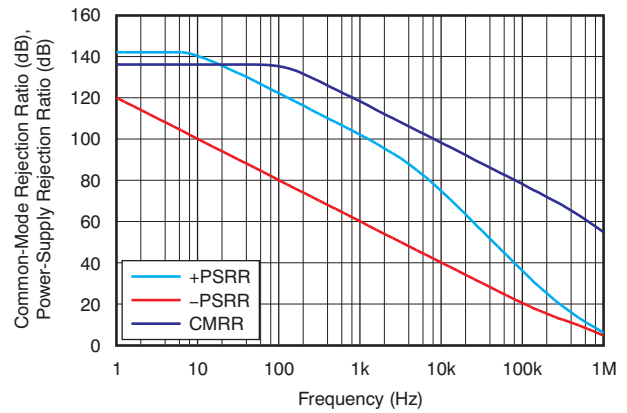


Figure 10. CMRR and PSRR vs Frequency (Referred-to-Input)

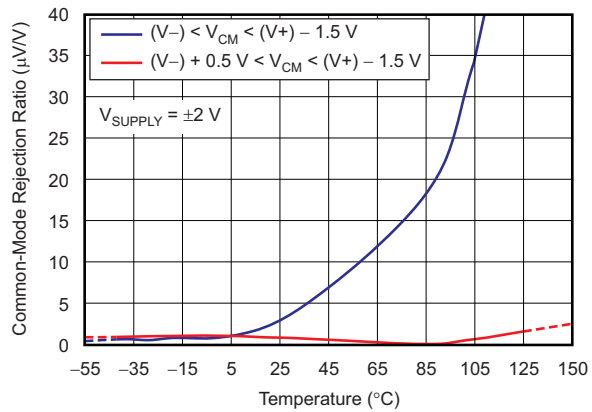


Figure 11. CMRR vs Temperature

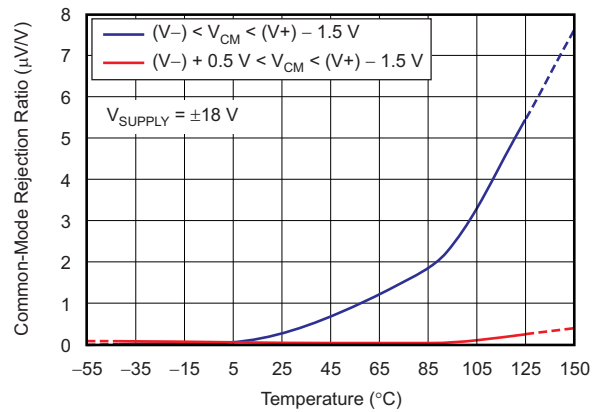
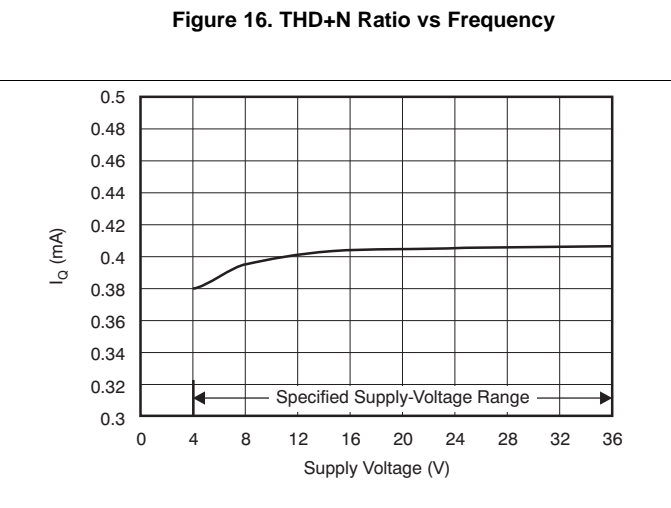
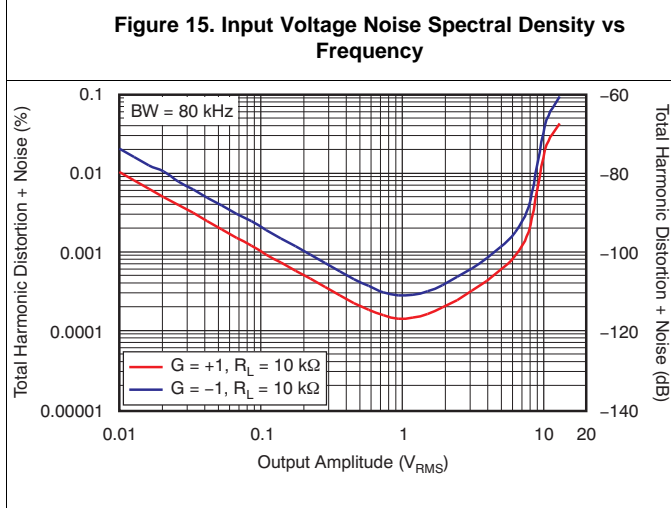
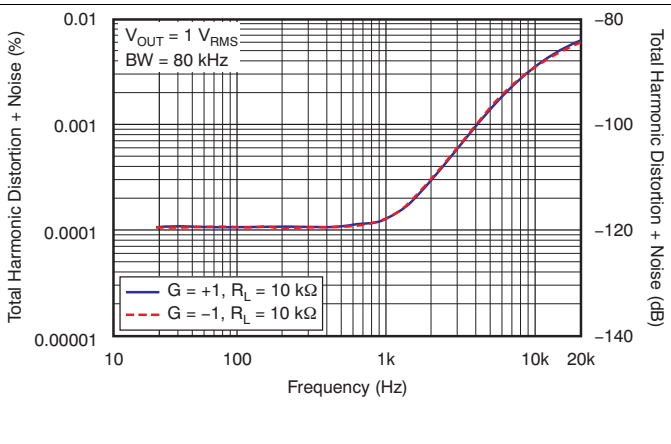
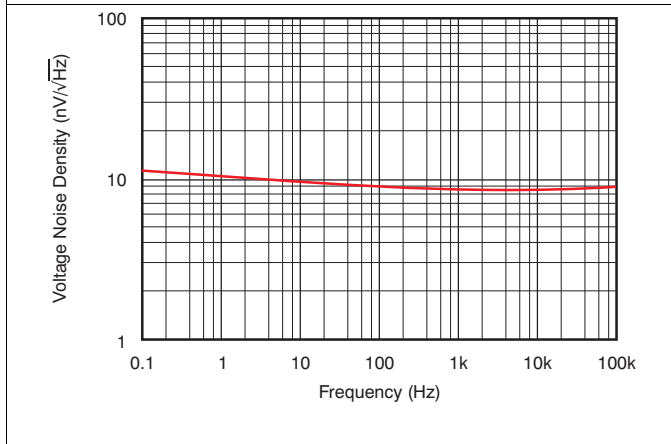
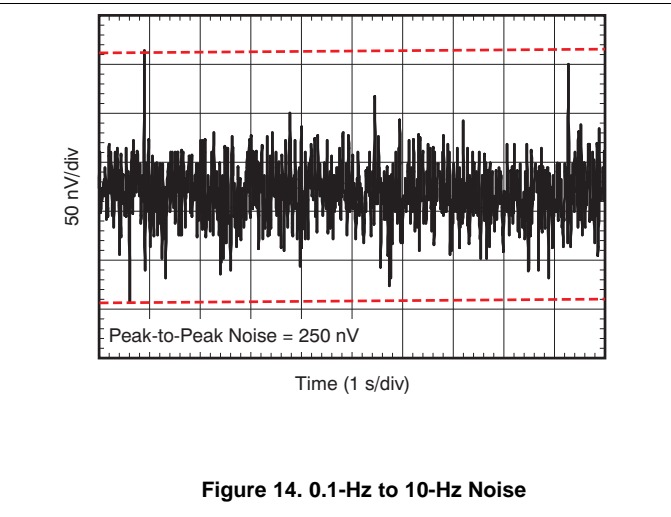
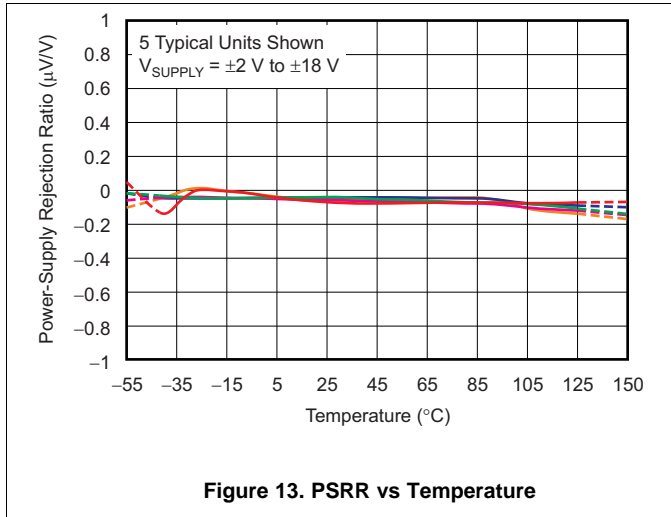


Figure 12. CMRR vs Temperature

$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.



$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.

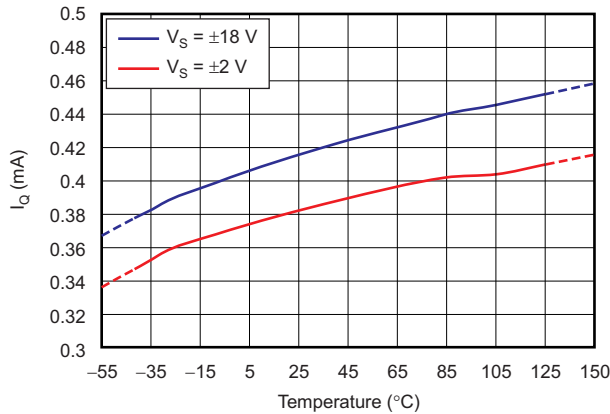


Figure 19. Quiescent Current vs Temperature

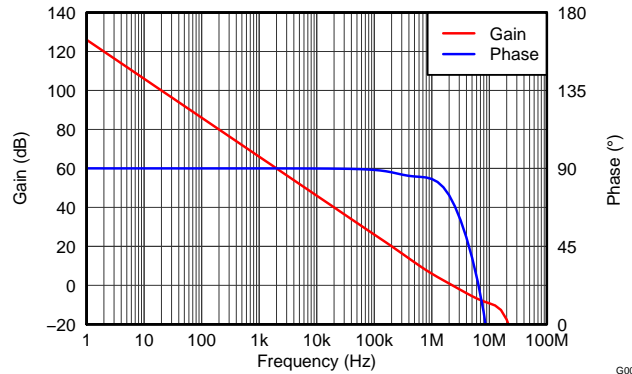


Figure 20. Open-Loop Gain and Phase vs Frequency

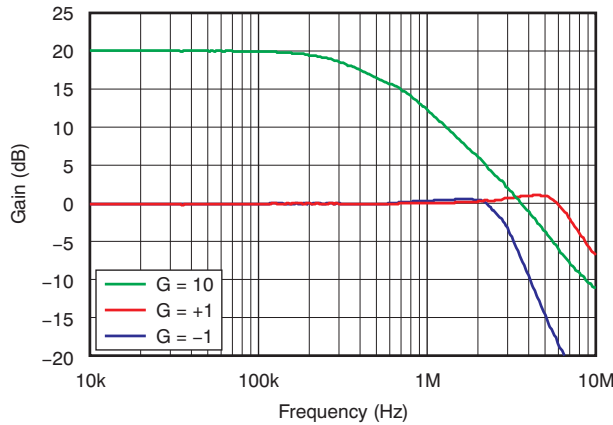


Figure 21. Closed-Loop Gain vs Frequency

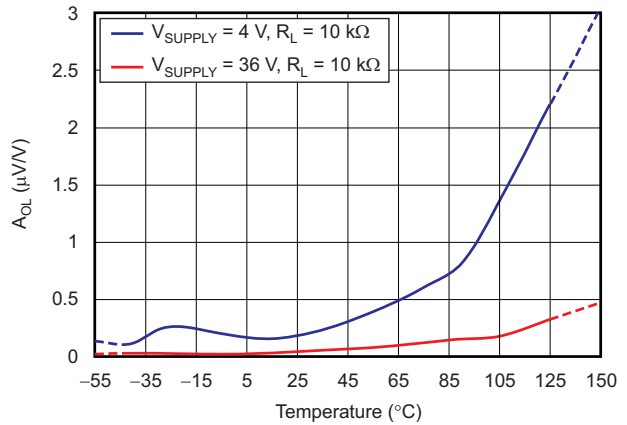


Figure 22. Open-Loop Gain vs Temperature

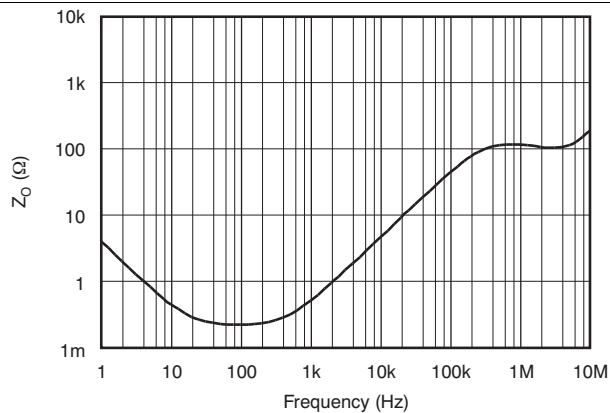


Figure 23. Open-Loop Output Impedance vs Frequency

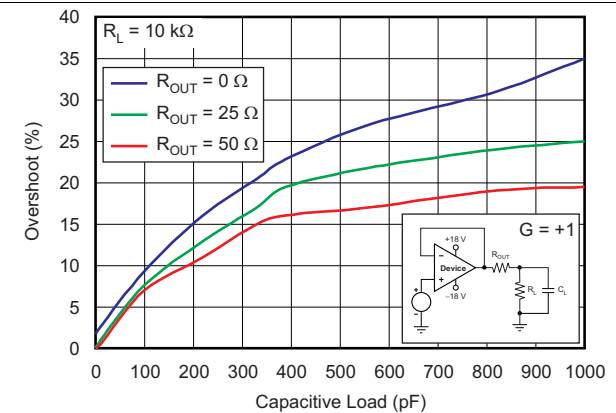


Figure 24. Small-Signal Overshoot vs Capacitive Load (100-mV Output Step)

$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.

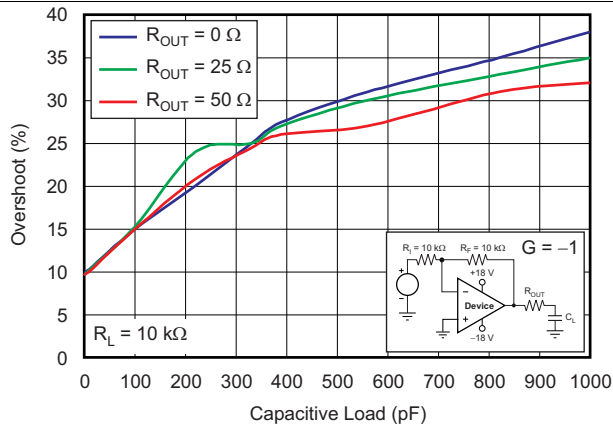


Figure 25. Small-Signal Overshoot vs Capacitive Load (100-mV Output Step)

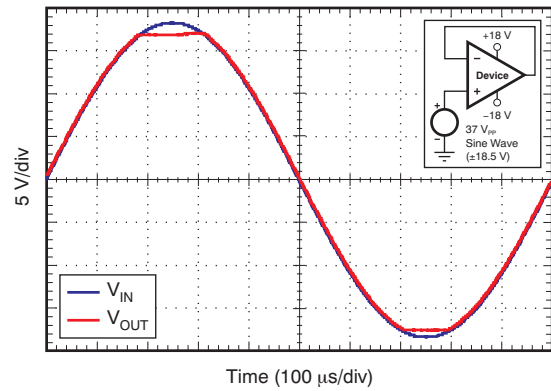


Figure 26. No Phase Reversal

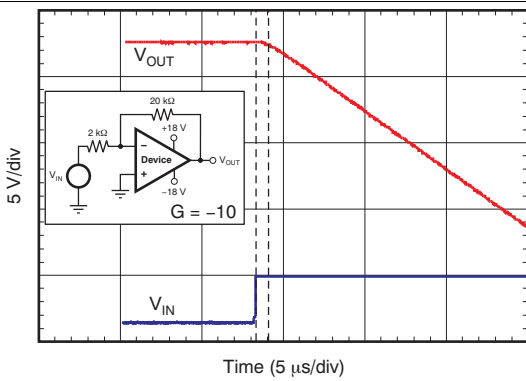


Figure 27. Positive Overload Recovery

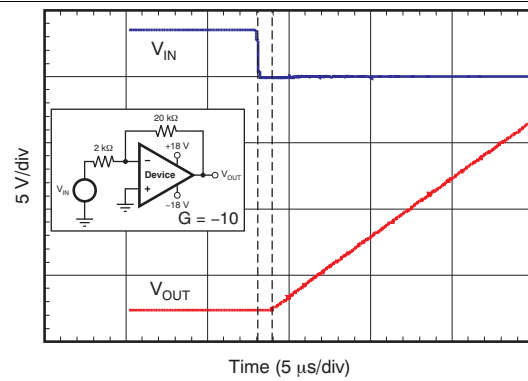


Figure 28. Negative Overload Recovery

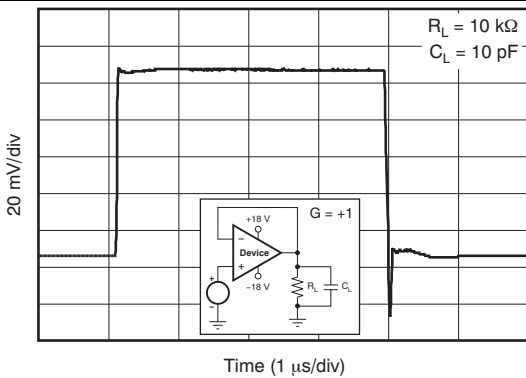


Figure 29. Small-Signal Step Response (100 mV)

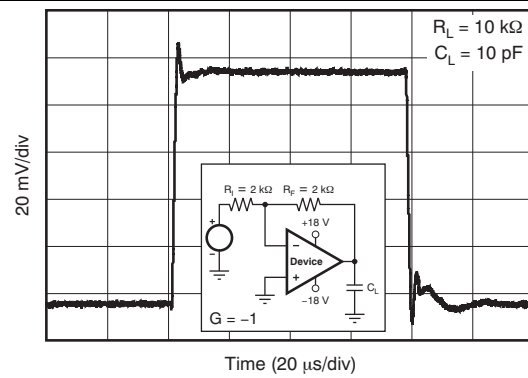


Figure 30. Small-Signal Step Response (100 mV)

$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.

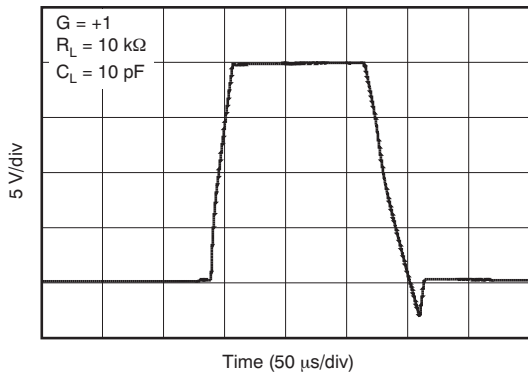


Figure 31. Large-Signal Step Response

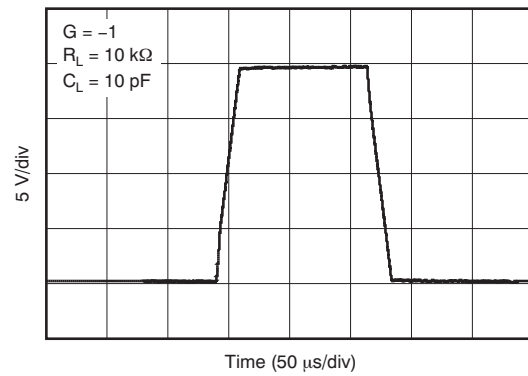


Figure 32. Large-Signal Step Response

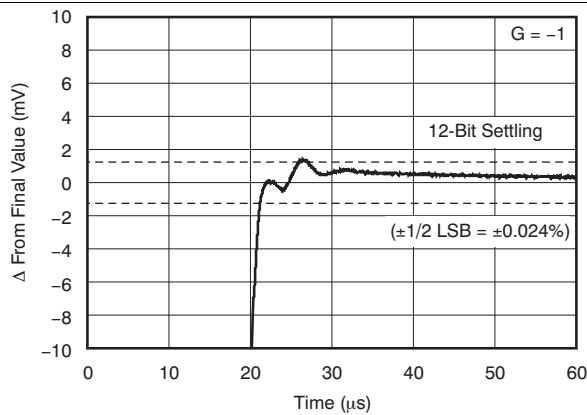


Figure 33. Large-Signal Settling Time (10-V Positive Step)

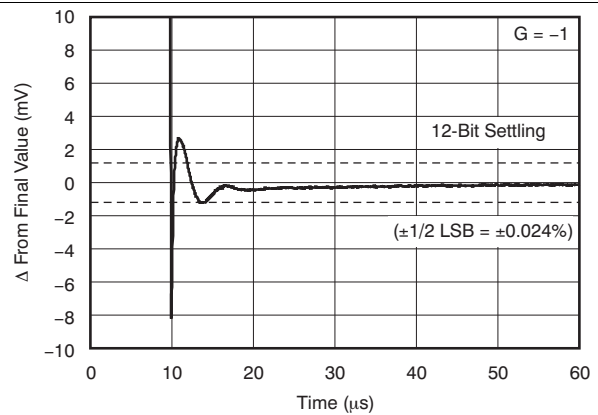


Figure 34. Large-Signal Settling Time (10-V Negative Step)

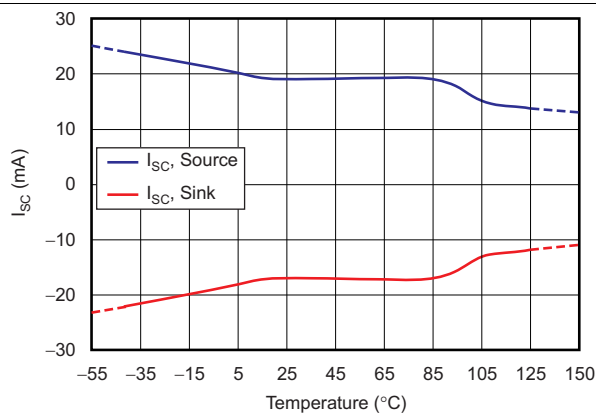


Figure 35. Short Circuit Current vs Temperature

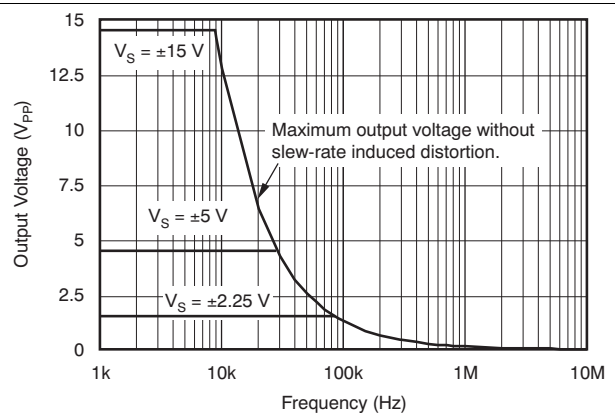


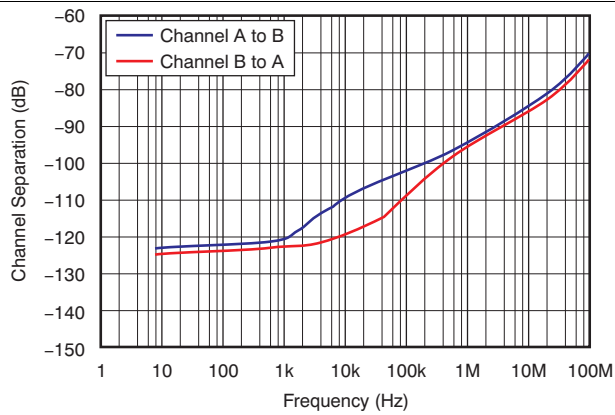
Figure 36. Maximum Output Voltage vs Frequency

**OPA4188**

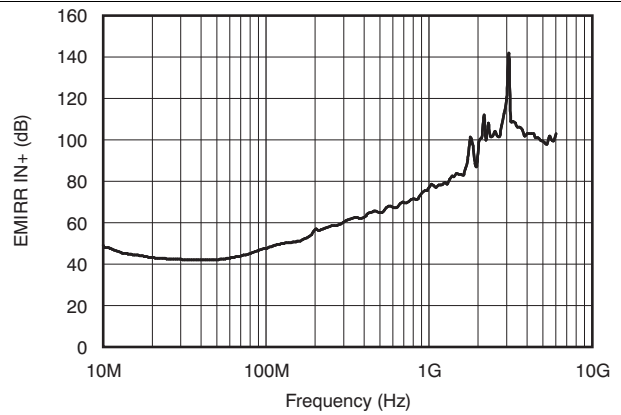
ZHCS959D – JUNE 2012 – REVISED SEPTEMBER 2016

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$V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$ , unless otherwise noted.



**Figure 37. Channel Separation vs Frequency**



**Figure 38. EMIRR IN+ vs Frequency**

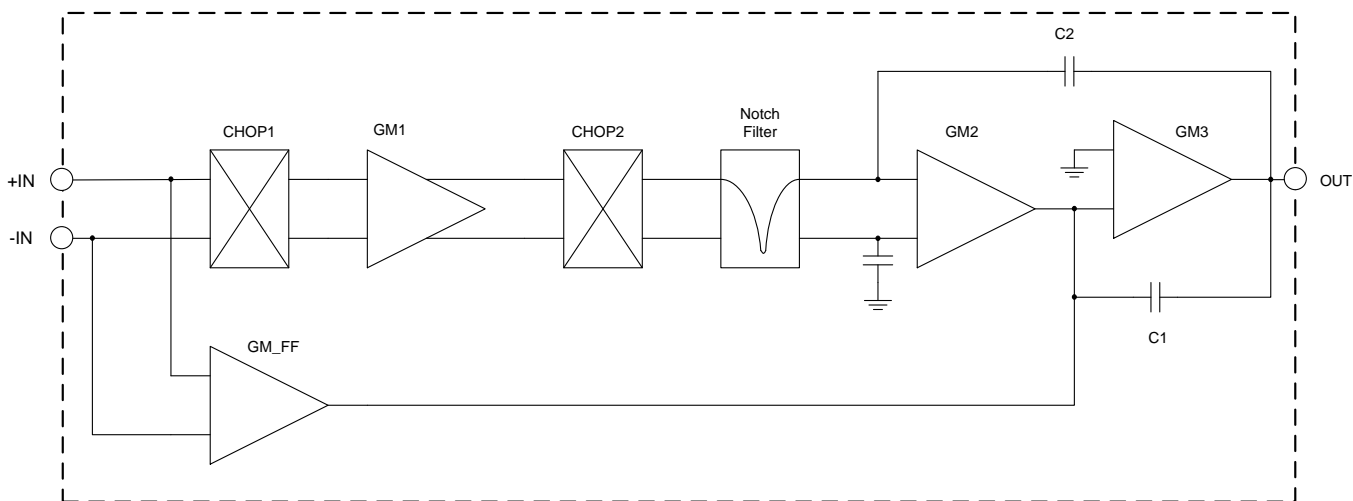


## 8 Detailed Description

### 8.1 Overview

The OPA4188 operational amplifier combines precision offset and drift with excellent overall performance, making the device ideal for many precision applications. The precision offset drift of only 0.085  $\mu\text{V}$  per degree Celsius provides stability over the entire temperature range. In addition, the device offers excellent overall performance with high CMRR, PSRR, and AOL. As with all amplifiers, applications with noisy or high-impedance power supplies require decoupling capacitors close to the device pins. In most cases, 0.1- $\mu\text{F}$  capacitors are adequate. The OPA4188 device is developed using TI's proprietary auto-zero architecture shown in [Functional Block Diagram](#). The internal synchronous notch filter removes switching noise from the CHOP1 and CHOP2 stages, resulting in a low noise density of 8.8  $\text{nV}/\sqrt{\text{Hz}}$ , low input offset voltage maximum of only 25  $\mu\text{V}$ . Input offset drift maximum of only 0.085  $\mu\text{V}/^\circ\text{C}$  allows for calibration free system design.

### 8.2 Functional Block Diagram



### 8.3 Feature Description

#### 8.3.1 Phase-Reversal Protection

The OPA4188 device has an internal phase-reversal protection. Many op amps exhibit a phase reversal when the input is driven beyond its linear common-mode range. This condition is most often encountered in noninverting circuits when the input is driven beyond the specified common-mode voltage range, causing the output to reverse into the opposite rail. The OPA4188 input prevents phase reversal with excessive common-mode voltage. Instead, the output limits into the appropriate rail. This performance is shown in [Figure 39](#).

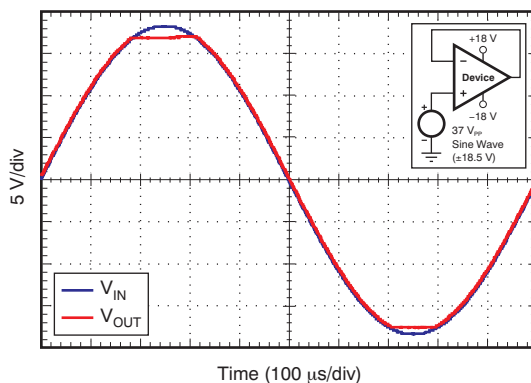
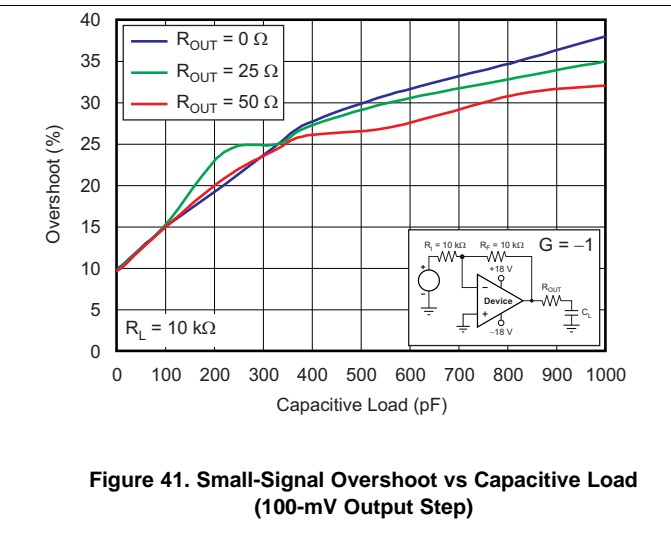
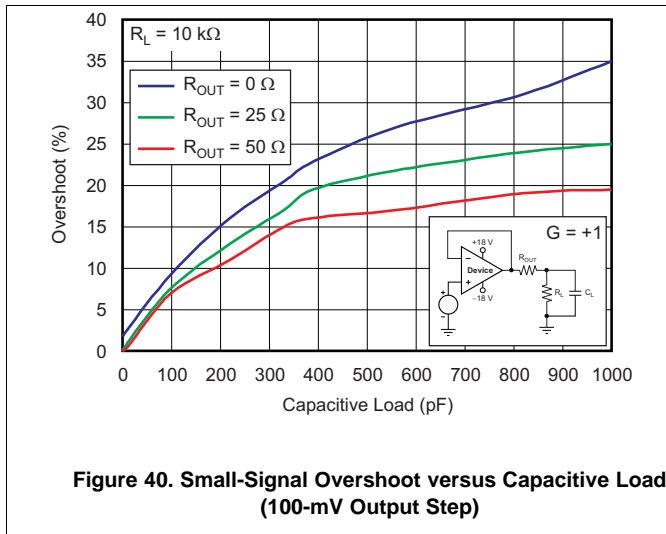


Figure 39. No Phase Reversal

## Feature Description (continued)

### 8.3.2 Capacitive Load and Stability

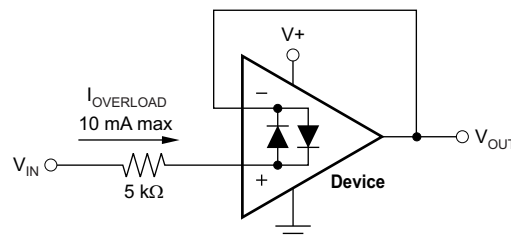
The OPA4188 dynamic characteristics have been optimized for a range of common operating conditions. The combination of low closed-loop gain and high capacitive loads decreases the amplifier phase margin and can lead to gain peaking or oscillations. As a result, heavier capacitive loads must be isolated from the output. The simplest way to achieve this isolation is to add a small resistor (for example,  $R_{OUT}$  equal to  $50\ \Omega$ ) in series with the output. Figure 40 and Figure 41 illustrate graphs of small-signal overshoot versus capacitive load for several values of  $R_{OUT}$ . For details of analysis techniques and application circuits, see [Feedback Plots Define Op Amp AC Performance](#), available for download from [www.ti.com](http://www.ti.com).



### 8.3.3 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

These ESD protection diodes also provide in-circuit, input overdrive protection, as long as the current is limited to 10 mA as stated in the [Absolute Maximum Ratings](#). Figure 42 shows how a series input resistor may be added to the driven input to limit the input current. The added resistor contributes thermal noise at the amplifier input and its value should be kept to a minimum in noise-sensitive applications.



**Figure 42. Input Current Protection**

An ESD event produces a short-duration, high-voltage pulse that is transformed into a short-duration, high-current pulse as it discharges through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent it from being damaged. The energy absorbed by the protection circuitry is then dissipated as heat.

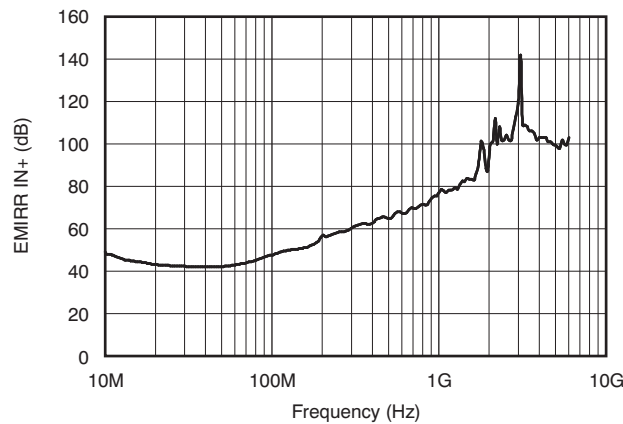
### Feature Description (continued)

When the operational amplifier connects into a circuit, the ESD protection components are intended to remain inactive and not become involved in the application circuit operation. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. Should this condition occur, there is a risk that some of the internal ESD protection circuits may be biased on, and conduct current. Any such current flow occurs through ESD cells and rarely involves the absorption device.

If there is an uncertainty about the ability of the supply to absorb this current, external Zener diodes may be added to the supply pins. The Zener voltage must be selected such that the diode does not turn on during normal operation. However, its Zener voltage should be low enough so that the Zener diode conducts if the supply pin begins to rise above the safe operating supply voltage level.

#### 8.3.4 EMI Rejection

The OPA4188 device uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI interference from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the OPA4188 benefits from these design improvements. Texas Instruments has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. Figure 43 shows the results of this testing on the OPA4188 device. Detailed information can also be found in *EMI Rejection Ratio of Operational Amplifiers* available for download from [www.ti.com](http://www.ti.com).



**Figure 43. EMIRR Testing**

#### 8.4 Device Functional Modes

The OPA4188 device has a single functional mode that is operational when the power-supply voltage is greater than 4 V ( $\pm 2$  V). The maximum power supply voltage for the OPA4188 is 36 V ( $\pm 18$  V).

## 9 Applications and Implementation

### NOTE

Information in the following applications and implementation sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

The OPA4188 operational amplifier combines precision offset and drift with excellent overall performance, making it ideal for many precision applications. The precision offset drift of only 0.085  $\mu\text{V}$  per degree Celsius provides stability over the entire temperature range. In addition, the device offers excellent overall performance with high CMRR, PSRR, and  $A_{OL}$ . As with all amplifiers, applications with noisy or high-impedance power supplies require decoupling capacitors close to the device pins. In most cases, 0.1- $\mu\text{F}$  capacitors are adequate.

The application examples of [Figure 46](#) and [Figure 47](#) highlight only a few of the circuits where the OPA4188 device can be used.

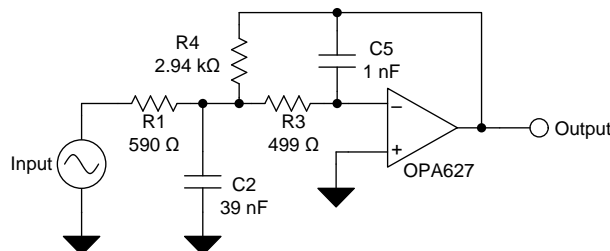
#### 9.1.1 Operating Characteristics

The OPA4188 device is specified for operation from 4 V to 36 V ( $\pm 2$  V to  $\pm 18$  V). Many of the specifications apply from  $-40^\circ\text{C}$  to  $125^\circ\text{C}$ . Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the [Typical Characteristics](#).

### 9.2 Typical Applications

#### 9.2.1 Second Order Low Pass Filter

Low pass filters are commonly employed in signal processing applications to reduce noise and prevent aliasing. The OPA4188 device is ideally suited to construct a high precision active filter. [Figure 44](#) illustrates a second order low pass filter commonly encountered in signal processing applications.



**Figure 44. 25-kHz Low Pass Filter**

##### 9.2.1.1 Design Requirements

Use the following parameters for this design example:

- Gain = 5 V/V (inverting gain)
- Low-pass cutoff frequency = 25 kHz
- Second order Chebyshev filter response with 3-dB gain peaking in the passband

##### 9.2.1.2 Detailed Design Procedure

The infinite-gain multiple-feedback circuit for a low-pass network function is shown in [Figure 44](#). Use [Equation 1](#) to calculate the voltage transfer function.

$$\frac{\text{Output}}{\text{Input}}(s) = \frac{-1/R_1 R_3 C_2 C_5}{s^2 + (s/C_2)(1/R_1 + 1/R_3 + 1/R_4) + 1/R_3 R_4 C_2 C_5} \quad (1)$$

### Typical Applications (continued)

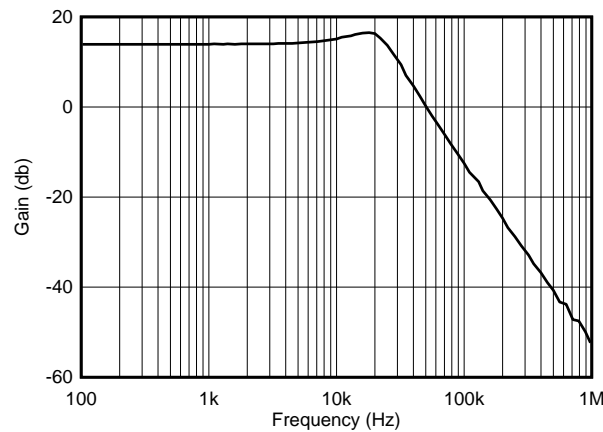
This circuit produces a signal inversion. For this circuit, use [Equation 2](#) to calculate the gain at DC and the low-pass cutoff frequency.

$$\text{Gain} = \frac{R_4}{R_1}$$

$$f_C = \frac{1}{2\pi} \sqrt{\frac{1}{R_3 R_4 C_2 C_5}} \tag{2}$$

Software tools are readily available to simplify filter design. [WEBENCH® Filter Designer](#) is a simple, powerful, and easy-to-use active filter design program. The WEBENCH Filter Designer lets you create optimized filter designs using a selection of TI operational amplifiers and passive components from TI's vendor partners. Available as a web based tool from the WEBENCH® Design Center, WEBENCH® Filter Designer allows you to design, optimize, and simulate complete multi-stage active filter solutions within minutes.

#### 9.2.1.3 Application Curve



**Figure 45. Gain (dB) vs Frequency (Hz)**

#### 9.2.2 Discrete INA + Attenuation for ADC With a 3.3-V Supply

[Figure 46](#) illustrates a circuit with high input impedance that can accommodate  $\pm 2$  V differential input signals. The output,  $V_{OUT}$ , is scaled into the full scale input range of a 3.3 V analog to digital converter. Input common mode voltages as high as  $\pm 10$  V can be present with no signal clipping. Input stage gain is determined by resistors  $R_5$ ,  $R_G$  and  $R_7$  according to [Equation 3](#).

$$\text{Gain} = 0.2x \frac{(R_5 + R_7)}{R_G} \tag{3}$$

Typical Applications (continued)

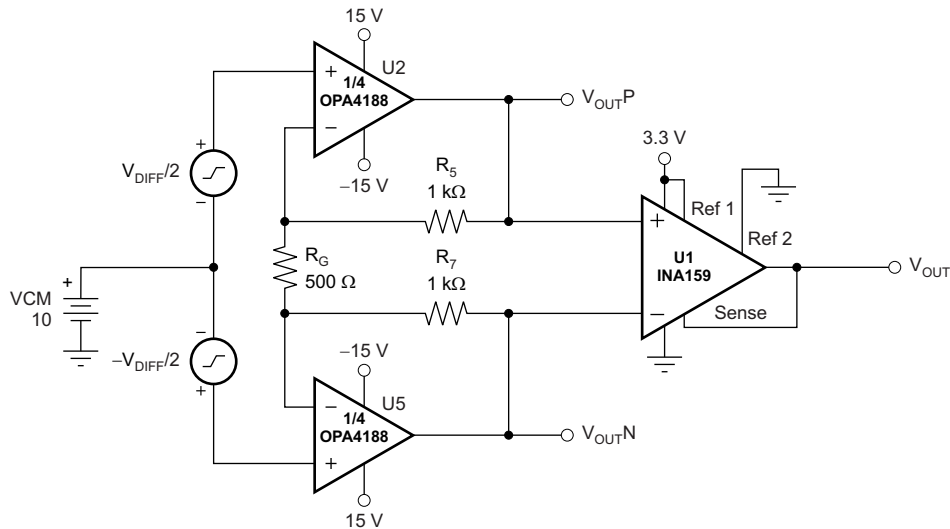
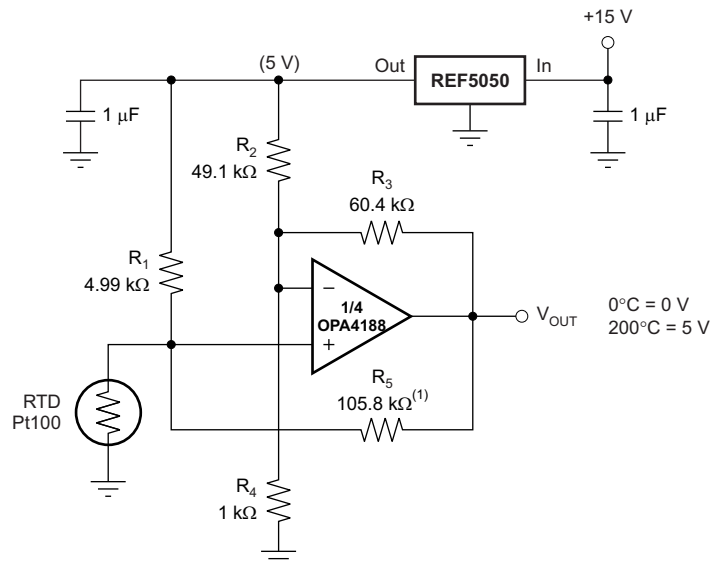


Figure 46. Discrete INA + Attenuation for ADC With a 3.3-V Supply Circuit

9.2.3 RTD Amplifier With Linearization

The OPA4188 device with ultra-low input offset voltage and ultra-low input offset voltage drift is ideally suited for RTD signal conditioning. Figure 47 illustrates a Pt100 RTD with excitation provided by a voltage reference and resistor R<sub>1</sub>. Linearization is provided by R<sub>5</sub>. Gain is determined by R<sub>2</sub>, R<sub>3</sub> and R<sub>4</sub>. The circuit is configured such that the output, V<sub>OUT</sub>, ranges from 0 V to 5 V over the temperature range from 0°C to 200°C. The OPA4188 requires split power supplies (±5.35 V to ±15 V) for proper operation in this configuration.



(1) R<sub>5</sub> provides positive-varying excitation to linearize output.

Figure 47. RTD Amplifier With Linearization Circuit

## 10 Power Supply Recommendations

The OPA4188 device is specified for operation from 4 V to 36 V ( $\pm 2$  V to  $\pm 18$  V); many specifications apply from  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$  and  $-55^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ . Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the [Typical Characteristics](#). Low-loss, 0.1- $\mu\text{F}$  bypass capacitors should be connected between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable to single-supply applications.

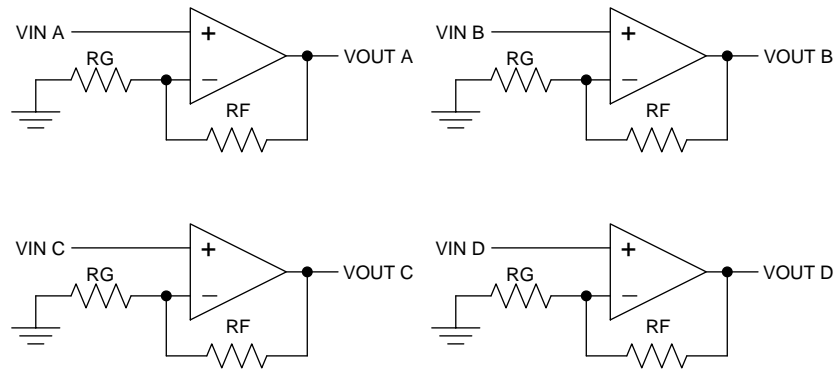
## 11 Layout

### 11.1 Layout Guidelines

For best operational performance of the device, use good PCB layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and operational amplifier itself. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1- $\mu\text{F}$  ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
  - The OPA6x7 is capable of high-output current (in excess of 45 mA). Applications with low impedance loads or capacitive loads with fast transient signals demand large currents from the power supplies. Larger bypass capacitors such as 1- $\mu\text{F}$  solid tantalum capacitors may improve dynamic performance in these applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds paying attention to the flow of the ground current. For more detailed information, see [Circuit Board Layout Techniques](#).
- To reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better as opposed to in parallel with the noisy trace.
- Place the external components as close to the device as possible. As shown in [Figure 48](#), keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.
- The case (TO-99 metal package only) is internally connected to the negative power supply, as with most common operational amplifiers.
- Pin 8 of the plastic PDIP, SOIC, and TO-99 packages has no internal connection.
- Cleaning the PCB following board assembly is recommended for best performance.
- Any precision integrated circuit may experience performance shifts due to moisture ingress into the plastic package. Following any aqueous PCB cleaning process, baking the PCB assembly is recommended to remove moisture introduced into the device packaging during the cleaning process. A low temperature, post cleaning bake at  $85^{\circ}\text{C}$  for 30 minutes is sufficient for most circumstances.

### 11.2 Layout Example



(Schematic Representation)

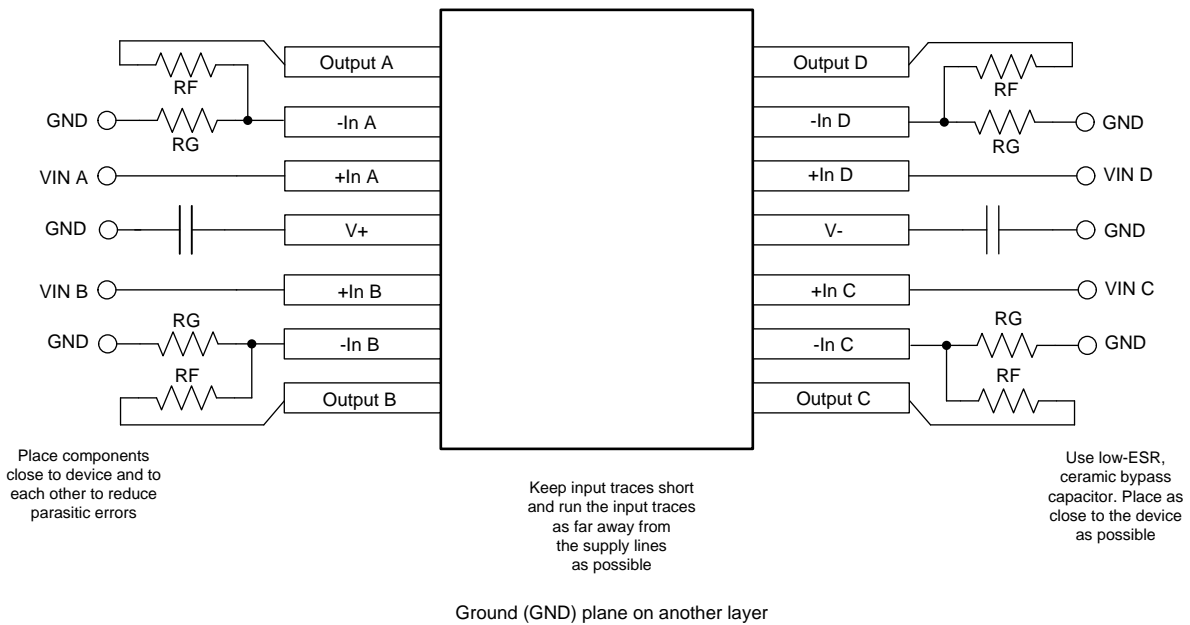


Figure 48. OPA4188 Layout Example



## 12 器件和文档支持

### 12.1 文档支持

#### 12.1.1 器件支持

##### 12.1.1.1 开发支持

###### 12.1.1.1.1 TINA-TI™ (免费软件下载)

TINA™是一款简单、功能强大且易于使用的电路仿真程序，此程序基于 SPICE 引擎。TINA-TI 是 TINA 软件的一款免费全功能版本，除了一系列无源和有源模型外，此版本软件还预先载入了一个宏模型库。TINA-TI 提供所有传统的 SPICE 直流 (DC)、瞬态和频域分析以及其他设计功能。

TINA-TI 可从 Analog eLab Design Center (模拟电子实验室设计中心) [免费下载](#)，它提供全面的后续处理能力，使得用户能够以多种方式形成结果。虚拟仪器提供选择输入波形和探测电路节点、电压和波形的功能，从而创建一个动态的快速入门工具。

#### 注

这些文件需要安装 TINA 软件 (由 DesignSoft™提供) 或者 TINA-TI 软件。请从 [TINA-TI 文件夹](#) 中下载免费的 TINA-TI 软件。

###### 12.1.1.1.2 TI 高精度设计

OPAx188 器件 (或类似运算放大器) 采用多种 TI 高精度设计。如需获取相关内容，请访问 <http://www.ti.com/ww/en/analog/precision-designs/>。TI 高精度设计是由 TI 公司高精度模拟应用专家创建的模拟解决方案，提供了许多实用电路的工作原理、组件选择、仿真、完整印刷电路板 (PCB) 电路原理图和布局布线、物料清单以及性能测量结果。

###### 12.1.1.1.3 WEBENCH® Filter Designer

**WEBENCH® 滤波器设计器**是一款简单、功能强大且便于使用的有源滤波器设计程序。WEBENCH® Filter Designer 允许用户通过选择 TI 运算放大器以及 TI 供应商合作伙伴的无源组件来构建优化滤波器设计方案。

WEBENCH® 设计中心以基于网络的工具形式提供 **WEBENCH® Filter Designer**。用户通过该工具可在短时间内完成多级有源滤波器解决方案的设计、优化和仿真。

### 12.1.2 相关文档

相关文档如下：

- 《电路板布局布线技巧》 (文献编号：SLOA089)。
- 《适用于所有人的运算放大器》 (文献编号：SLOD006)。
- 《运算放大器增益稳定性的第 3 部分：交流增益误差分析》 (文献编号：SLYT383)。
- 《运算放大器增益稳定性的第 2 部分：直流增益误差分析》 (文献编号：SLYT374)。
- 《在全差分有源滤波器中使用无限增益、MFB 滤波器拓扑》 (文献编号：SLYT343)。
- 《运算放大器性能分析》 (文献编号：SBOA054)。
- 《运算放大器的单电源运行》 (文献编号：SBOA059)。
- 《调整放大器》 (文献编号：SBOA067)。
- 《无铅组件涂层的保存期评估》 (文献编号：SZZA046)。

## 12.2 商标

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### 12.3 静电放电警告



ESD 可能会损坏该集成电路。德州仪器 (TI) 建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序，可能会损坏集成电路。

ESD 的损坏小至导致微小的性能降级，大至整个器件故障。精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

### 12.4 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

### 13 机械、封装和可订购信息

以下页中包括机械、封装和可订购信息。这些信息是针对指定器件可提供的最新数据。这些数据会在无通知且不对本文档进行修订的情况下发生改变。欲获得该数据表的浏览器版本，请查阅左侧的导航栏。

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
OPA4188AID	ACTIVE	SOIC	D	14	50	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA4188	<a href="#">Samples</a>
OPA4188AIDR	ACTIVE	SOIC	D	14	2500	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA4188	<a href="#">Samples</a>
OPA4188AIPW	ACTIVE	TSSOP	PW	14	90	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA4188	<a href="#">Samples</a>
OPA4188AIPWR	ACTIVE	TSSOP	PW	14	2000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA4188	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) **MSL, Peak Temp.** - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) **Lead finish/Ball material** - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA4188AIDR	SOIC	D	14	2500	330.0	16.4	6.5	9.0	2.1	8.0	16.0	Q1
OPA4188AIPWR	TSSOP	PW	14	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA4188AIDR	SOIC	D	14	2500	356.0	356.0	35.0
OPA4188AIPWR	TSSOP	PW	14	2000	356.0	356.0	35.0

**TUBE**


\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (μm)	B (mm)
OPA4188AID	D	SOIC	14	50	506.6	8	3940	4.32
OPA4188AIPW	PW	TSSOP	14	90	508	8.5	3250	2.8

D (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in inches (millimeters).
  - B. This drawing is subject to change without notice.
  - Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
  - Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
  - E. Reference JEDEC MS-012 variation AB.



D (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

PW (R-PDSO-G14)

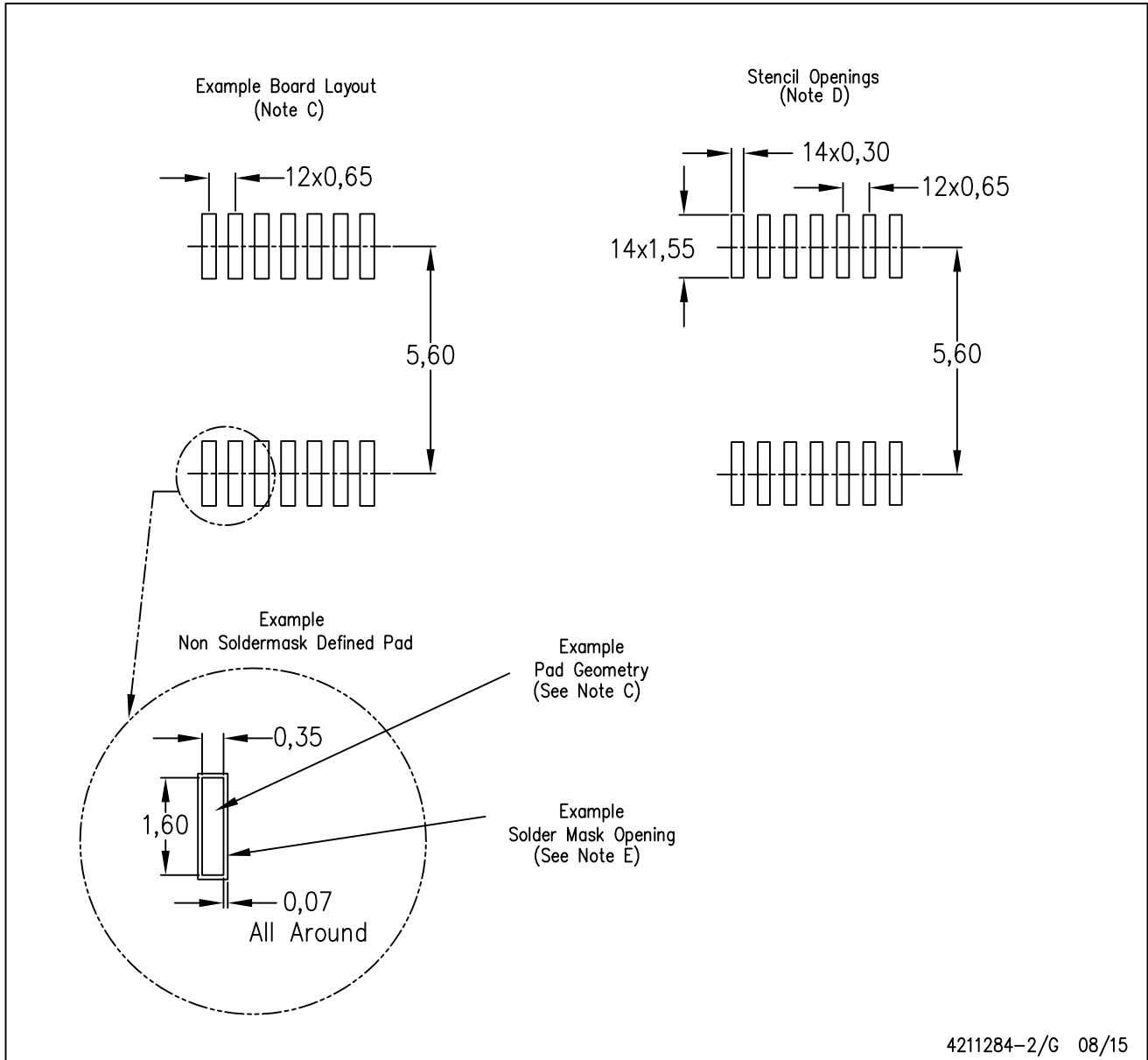
PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  - C. Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
  - D. Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
  - E. Falls within JEDEC MO-153

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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